



Engineering Assessment Report

Residential Development at Broomfield SHD Lands, Malahide

April 2022

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This document has been prepared and checked in accordance with
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Comments



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1. Introduction

1.1 Background of Report

This engineering assessment report has been prepared by Waterman Moylan as part of the planning documentation for a proposed residential development on lands at Broomfield, part of the Broomfield SHD lands, Malahide, Co. Dublin.

This report assesses wastewater and surface water drainage, water supply infrastructure and the road and transportation network in the vicinity of the site, and details the criteria used to design the proposed wastewater and surface water drainage, water supply and road networks.

1.2 Site Location and Description

The existing site access is from Back Road, 0.5km east of the junction of Back Road and Kinsealy Lane.

The overall proposed development is divided into 2 sites as indicated in *Figure 1* overleaf. The north site is located between the existing Ashwood Hall residential development to the west and the Dublin-Belfast rail line to the east. To the south is agricultural land, the north is bounded by existing residential properties fronting the Back Road.

The southern site is bound by the Hazelbrook development to the west, Brookfield development to the north and agricultural lands to the east. The southern boundary is formed by the Hazelbrook Stream.

The southern site is greenfield in nature. The northern site is predominantly greenfield and was the former location of a rugby club. There is a small area of hardstanding which was previously the club's car park, together with existing structures, formerly the clubhouse and outhouse. These have been extensively vandalised in the form of fire damage, and demolition of the remainder of the structures is included as part of the subject application. The subsoil in the area to the south of the former playing field is an infill area consisting of inert rubble which has been surveyed, sampled, and analysed. This rubble will be excavated and disposed of as appropriate. For further details please refer to the Preliminary Construction, Demolition & Waste Management Plan Report, submitted under a separate cover.

A topographic survey of the area indicated that the north site generally slopes uniformly from north-east to south, from a height of 20.5m to 11.5m, with an existing static ditch system along the south-east boundary, and ditch to the south-west. The southern site also slopes from north to south from a height of 6m to 4.7m with localised high points and has an existing ditch system along its north boundary and Hazelbrook Stream along the southern boundary.

The ditch systems referenced above join the Hazelbrook stream, which in turn outfalls to the Sluice River which in turn ultimately outfalls to the sea at Baldoyle Bay, C. 2.3km south-east of the subject site.

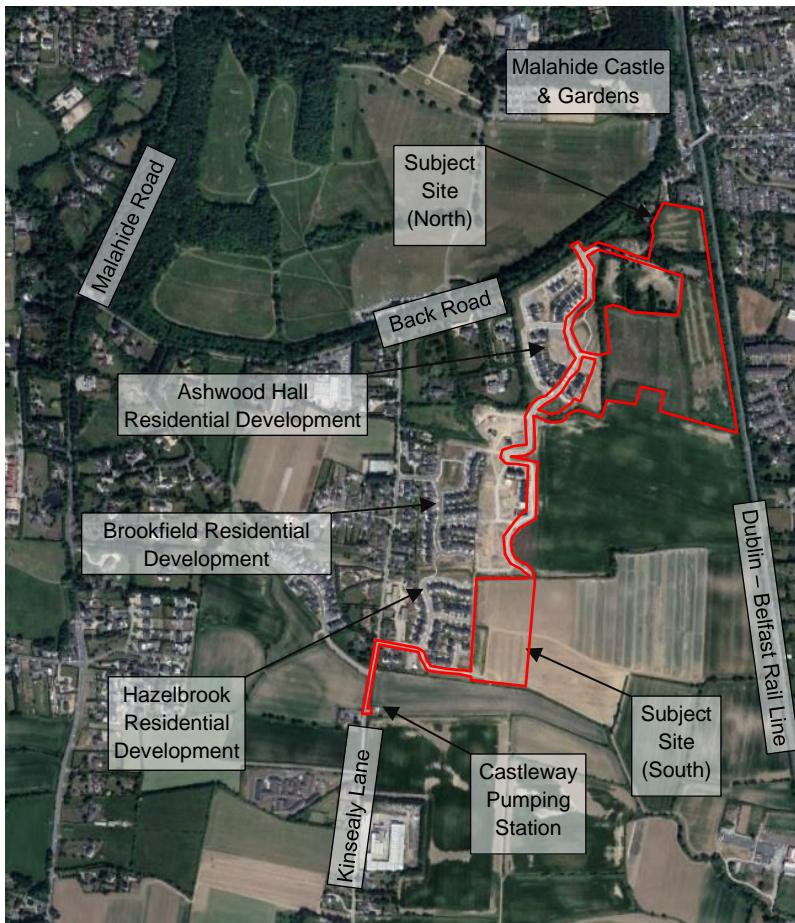


Figure 1 | Site Location (Source: Google Earth)

1.3 Proposed Development

The proposed development consists of a total of 415 No. residential units, comprising of 252 houses, 28 duplex units and 135 apartments as set out in the Schedule of Accommodation in *Table 1* below. The proposed development will also include the construction of a 476m² creche, projected to cater for 15 staff and 85 children.

Description	1-bed	2-bed	3-bed	4-bed	5-Bed	Total
House	-	-	192	48	12	252
Duplex	8	14	6	-	-	28
Apartment	37	93	5	-	-	135
Total	45	107	203	48	12	415

Table 1 | Schedule of Accommodation

The development includes all associated site works, undergrounding of overhead lines, boundary treatments, drainage, and service connections.

2. Foul Water Network

2.1 Existing Foul Water Network

The site is currently greenfield in nature. The adjacent residential developments, Hazelbrook & Ashwood Hall both have foul water spurs constructed for future connections to the proposed development. These existing developments drain by gravity in a south-westerly direction to the Kinsealy Lane sewer system, which in turn currently drains to Connolly Avenue pumping station. Connolly Avenue pumping station pumps north-eastwards to the gravity network in Malahide which ultimately drains to Malahide Wastewater Treatment Plant (WwTP).

It is noted that Connolly Avenue pumping station, the gravity foul water network in Malahide and Malahide WwTP all currently have capacity issues during heavy rainfall events.

2.2 Future Foul Water Network Upgrades

Irish Water have recently commissioned a new pumping station on Chapel Road discharging via a new rising main to the existing North Fringe Interceptor Sewer, at Marrsfield Avenue, Clongriffin. The Floraville pumping station, at the southern end of Kinsealy Lane has been decommissioned and will instead drain by gravity to the new Chapel Road pumping station. This has alleviated some of the constraints in the Connolly Avenue pumping station catchment.

During the pre-planning process in respect of this subject application, Irish Water further discussed the possibility of a new 'Castleway' pumping station on Kinsealy Lane, which would pump wastewater from the subject site and the surrounding area southwards to the newly commissioned gravity sewer at Chapel Road Pumping Station. This network has capacity available to serve the subject development and diverted flows from Connolly Avenue pumping station.

This long-term solution will relieve capacity constraints at Connolly Avenue Pumping Station, the Malahide foul water gravity network and within the Malahide WWTP catchment area, and this has been designed and sized to accommodate this subject development.

This Castleway pumping station has received a full Grant of Permission from Fingal County Council on 21st January 2022 under Planning Register Reference No. F21A/0451.

A letter from the Applicant of the Castleway pumping station (Carley Properties Ltd.) has been obtained, and states that Carley Properties Ltd. intend to develop this pumping station. The letter also confers the legal entitlement to Birchwell Developments Ltd. to develop the pumping station if so required, to ensure this development is not reliant on a third party to construct the pumping station.

Construction of the pumping station will be completed prior to the connection of units from this subject application.

A Confirmation of Feasibility Letter was issued by Irish Water on 13 January 2021, and is included as Appendix A. The confirmation of feasibility letter states that connection to the Irish Water network is feasible subject to delivery of the new Castleway pumping station and commissioning of the Chapel Road pumping station. Once again, Chapel Road pumping Station has since been commissioned.

2.3 Proposed Foul Water Network

It is proposed to drain wastewater from the proposed development in a south-westerly direction by gravity through a series of 150mm, 225mm, & 300mm diameter sewer networks to the existing sewer network in the Ashwood and Hazelbrook developments. It is further proposed to upgrade part of the existing foul drainage network in the Hazelbrook development from a 225mm to a 300mm diameter pipe network. This will continue to drain by gravity to the existing public sewer in Kinsealy Lane, which in turn currently discharges to Connolly Avenue Pumping Station. As part of the construction of the Castleway pumping station, this foul water sewer is proposed to be diverted from Connolly Avenue pumping station to the Castleway pumping station.

The existing foul networks in the adjacent residential developments, have been appropriately designed and constructed, including spurs for connection points, to accommodate the future connection of the proposed development. Letters of consent from the adjacent development owners have been obtained permitting connections to these privately owned networks. Please refer to the accompanying submission from Downey Planning for copies of the Letters of Consent.

The proposed internal foul drainage network has been designed and sized in accordance with the Irish Water code of Practice for Wastewater Infrastructure and Standard Details. Please refer to Drawing numbers: 18-091-P201 to P206, which show the proposed foul drainage layout, and existing foul water networks in adjacent estates, and subsequent route to the Castleway pumping station.

A Statement of Design Acceptance has also been issued by Irish Water and is provided in Appendix B.

2.4 Foul Water Drainage Calculations

The calculated foul water flows at the subject development are set out in *Table 2*, below. Domestic wastewater loads have been calculated based on 2.7 persons per unit with a per capita wastewater flow of 150 litres per head per day along with a 10% unit consumption allowance, in line with Section 3.6 of the Irish Water Code of Practice for Wastewater Infrastructure. A peak flow multiplier of 3 has been used, as per Section 2.2.5 of Appendix B of the Code of Practice.

It is calculated that the creche will generate flow for 100 persons (15 staff and 85 children), with a wastewater volume of 90 litres per head per day, based on the figure for the most similar type of usage: a non-residential school with canteen facilities, also as per Appendix C of the Code of Practice.

Description	Total Population	Load per Capita	Daily Load	Total DWF	Peak Flow
	No. People	l/day	l/day	l/s	l/s
252 Houses	680.4	150	112,266	1.299	3.897
28 Duplexes	75.6	150	12,474	0.144	0.432
135 Apartments	364.5	150	60,142.5	0.696	2.088
Creche	100	90	9,900	0.115	0.345
Total	1,220.5	Varies	194,782.5	2.254	6.762

Table 2 | Calculation of Total Foul Water Flow from the Development

The total dry weather flow from the development has been calculated as: 2.254 l/s, with a peak flow of 6.762 l/s.

2.5 Foul Water Drainage – General

Foul water sewers will be constructed strictly in accordance with Irish Water requirements. No private drainage will be located within public areas.

Drains will be laid to comply with the requirements of the latest Building Regulations, and in accordance with the recommendations contained in the Technical Guidance Document H.

3. Surface Water Network

3.1 Existing Surface Water Network

Surface water from the site discharges into a series of boundary ditches on the perimeter of the sites. The southern catchment of the south site drains directly to the Hazelbrook Stream. Part of the northern site's drainage ditch network on the southern boundary is a static/dry ditch. The remainder of the ditches drain to the Hazelbrook Stream, which is a tributary of the Sluice River that ultimately outfalls to the sea at Baldoyle Bay. Baldoyle Bay has been designated as an SPA (Special Protection Area) by the NPWS (National Park and Wildlife Service) and Local authority, under the RAMSAR Convention. It was declared a Statutory Nature Reserve in 1988 and supports several habitats as listed in the EU Habitats Directive.

3.2 SuDS

Sustainable Drainage System (SuDS) are a collection of water management practices that aim to align modern drainage systems with natural water processes.

By using SuDS techniques, water is either infiltrated or conveyed more slowly to the drainage system and ultimately more slowly to water courses via permeable paving, swales, green roofs, rainwater harvesting, detention basins, ponds, and wetlands.

Fingal County Council's document titled Green/Blue Infrastructure for Development advises that: "*These facilities are designed to prevent pollution of streams and rivers and to slow down runoff from sites, therefore helping to prevent downstream flooding and improve water quality. This closely mimics natural catchment behaviour where rainfall either infiltrates through the soil or runs off slowly over the ground surface to the nearest watercourse. This is known as the "treatment train" approach. SuDS devices should be placed at source, site, and regional levels. SuDS can also provide amenity benefits to local communities and benefits for biodiversity simultaneously*".

In the following sections of the surface water chapter, it will be outlined in detail how SuDS devices have been utilised and incorporated to the overall plan for the proposed development, and how their inclusion will mitigate the risk of localised and downstream flooding, while also promoting residential amenity and biodiversity.

The Fingal County Council SuDS selection checklist is included as Appendix C.

3.3 Proposed Surface Water Network and SuDS Strategy

It is proposed to construct a SW drainage network that will service and attenuate the development internally before discharging at the current greenfield (or allowable) rates to the local natural ditch systems. Surface drainage layout and attenuation strategy can be reviewed on drawing numbers 18-091-P201, P202, P203 & P205.

The location and extent of SuDS devices proposed for the development can be viewed on drawing 18-091-P235 and described below in Sections 3.3.1 to 3.3.4.

For storm water management purposes, it is proposed to divide the site into eight separate sub-catchments, as shown in *Figures 2 & 3* overleaf.

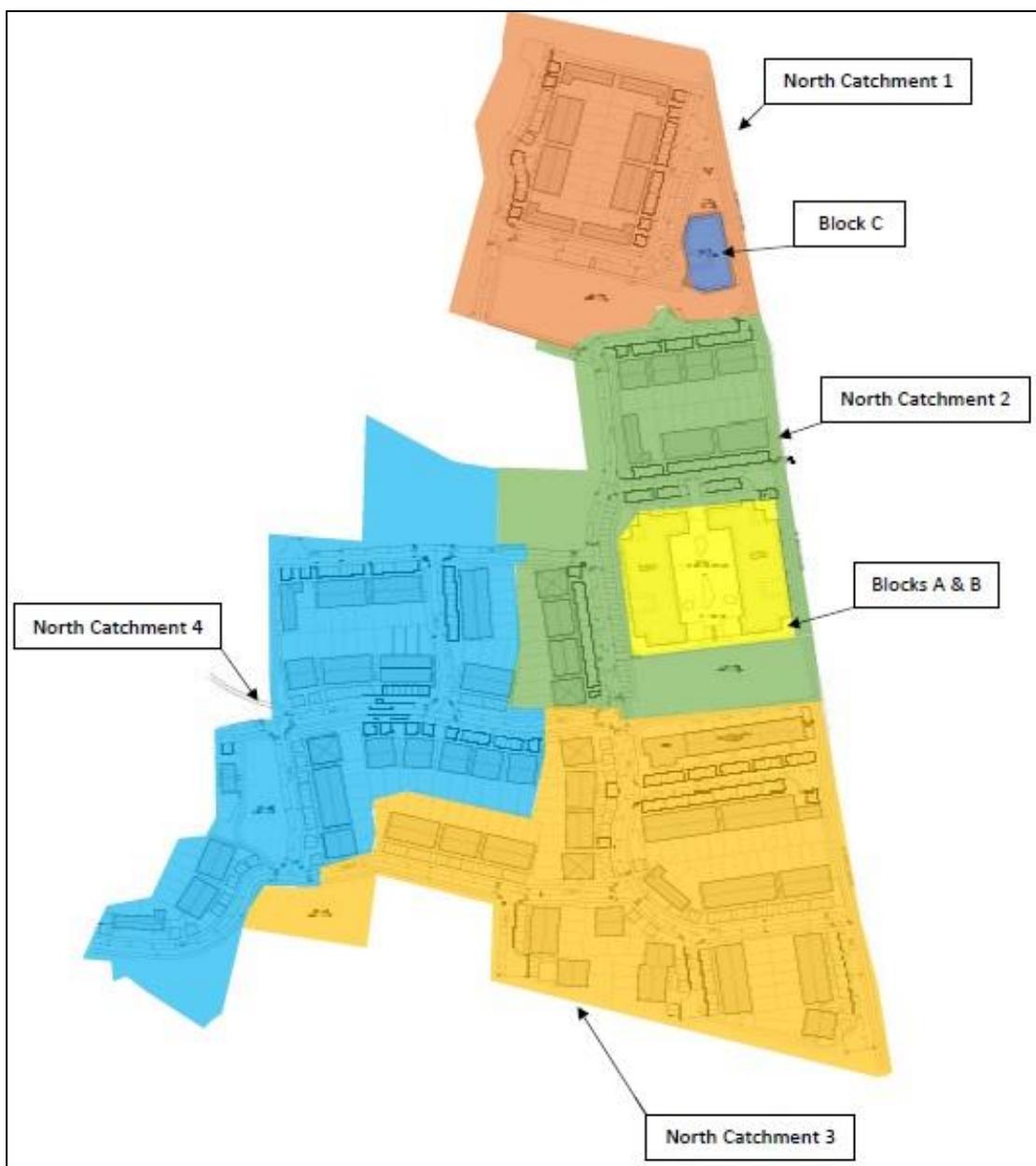


Figure 2 | Sketch of North Site Catchments



Figure 3 | Sketch of South Site Catchments

Storm water from each catchment will be attenuated and discharge at a controlled rate, limited to the greenfield equivalent runoff or 2 l/s/ha (whichever is greater), to ultimately outfall to the existing ditch system on the site, south catchment 2 however, will outfall directly to the Hazelbrook Stream. The proposed development will be designed to incorporate best drainage practice. Section 3.4, below, sets out the methodology used in determining the existing greenfield runoff rates and calculating attenuation storage requirements for the site.

It is proposed to incorporate a Storm Water Management Plan through the use of various SuDS techniques to treat and minimise surface water runoff from the site. The methodology involved in developing a Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin

Strategic Drainage Study (GDSDS) and in the SuDS Manual. Based on three key elements – Water Quantity, Water Quality and Amenity – the targets of the SuDS train concept have been implemented in the design, providing SuDS devices for each of the following:

- Source Control
- Site Control
- Regional Control

3.3.1 Source Control

Permeable Paving:

It is proposed to introduce permeable paving at all private driveways and parking courts throughout the development. Downpipes from the front of the houses and apartments will drain to filter drains beneath the permeable paving to facilitate maximum infiltration of surface water from driveways and roof areas.

The goal of permeable paving is to control stormwater at the source to reduce runoff. In addition to reducing surface runoff, permeable paving has the dual benefit of improving water quality by trapping suspended solids and filtering pollutants in the substrata layers.

Filter Drains:

It is proposed to install 225mm diameter filter drains, consisting of perforated pipes surrounded in filter stone around the perimeter of each apartment block. The filter drains will provide infiltration, optimise the retention time, and provide quality improvement to the storm water runoff, in particular the first flush from hardstanding areas. The proposed perforated pipes connect to the proposed surface water sewer network.

Green / Sedum Roof:

Section 3.6.7 of the Fingal County Council document Green/Blue Infrastructure for Development instructs that a green roof must be provided for a minimum of 60% of the total roof area, where it exceeds 300m², which in this case is applicable. It is proposed to introduce sedum roofing as a source control device on Apartment Blocks A, B, & C. The sedum roofing is proposed to cover a minimum of 60% of the total apartment roof area, totalling a cumulative green roof area of 1,949m². The sedum roofing typically consists of 75mm substrate with a sedum blanket.

The substrate and the plant layers in a green roof absorb large amounts of rainwater and release it back into the atmosphere by transpiration and evaporation. They also filter water as it passes through the layers, so the run-off, when it is produced, has fewer pollutants. Rainfall not retained by green roofs is detained, effectively increasing the time to peak, and slowing peak flows.

A sedum roof can reduce annual percentage runoff by between 40% and 80% through this retention and evapotranspiration, with the impact dependent on a range of factors including the depth of substrate, the saturation of substrate at the onset of a rain event, the angle of the roof, the range of vegetation growing, intensity of rainfall and the time of year.

A paper entitled *Green Roofs Over Dublin: A Green Roof Policy Guidance Paper for Dublin* was published in August 2008 with guidelines for Dublin City Council to develop planning directives for the incorporation of green roofs in new development. The table overleaf is taken from this document and shows the percentage of total rainfall retention over a 14-month period for different green roof treatments.

Slope	Media Depth	Light Rain <2mm	Medium Rain 2mm-6mm	Heavy Rain >6mm	Overall
2.0%	25mm	95.1%	82.9%	64.7%	69.8%
2.0%	40mm	97.1%	85.5%	65.1%	70.1%
6.5%	40mm	94.9%	83.1%	59.5%	65.9%
6.5%	60mm	95.8%	84.6%	62.0%	68.1%

Table 3 | Percentage of Total Rainfall Retention Over a 14-Month Period (Aug 2002-Oct 2003)

The proposed sedum roofing shall be on flat roofs with 2% slope with a media depth of 75mm, exceeding the depths shown above. Thus, the percentage of total rainfall retention can be expected to exceed the tabulated figures.

3.3.2 Site Control

Roadside Bio-retention Tree Pits:

It is proposed to provide roadside trees throughout the development. Trees can help control storm water runoff because their leaves, stems, and roots slow rain from reaching the ground and capture and store rainfall to be released later. Trees help to attenuate flows, trap silts and pollutants, promote infiltration and prevent erosion. Incorporating tree planting offers multiple benefits, including attractive planting features, improved air quality and increased biodiversity whilst helping to ensure adaptation to climate change.

Swales:

Swales are grassed channels proposed to run parallel and adjacent to selected roads throughout the site. Rainfall from the road surface will be directed to gaps in the road kerbing and will flow to the swales. The swales will be linked back to the drainage network to prevent flooding in extreme weather events, where the volume of rainfall exceeds the percolation capacity of the swales.

Grassed swales enhance surface water runoff quality as they slow down water flow, allowing suspended particles to filter and settle out of suspension.

The inclusion of swales is as requested by Fingal County Council during an online meeting in order to provide additional surface SuDS, to mitigate against the requirement for underground attenuation tanks to be utilised by the development.

3.3.3 Regional Control

Detention Basin / Underground Attenuation System:

Detention basins were investigated to store and attenuate the surface water volumes calculated to be generated by the development. While generally a preferred option, in this specific situation due to existing site topography and surrounding ditch network, they would require engineering deep depressions into open spaces rendering them generally unusable for the provision of other general amenities, as they would full with surface water during heavy rainfall events and would remain unusable for a number of days after, and further goes against Fingal County Council's objective of keeping all SUDS's areas under 10% of the site green area. As such, detention basins are not proposed and instead attenuation tanks will be utilised as the more suitable attenuation strategy.

An online meeting was held between Waterman Moylan and Fingal County Council Drainage Department and Parks Department on 6 May 2021 (after the Tri-partite meeting). At this meeting, Fingal County Council advised that given the constraints; that while above ground attenuation is their preference, that in this instance attenuation tanks (see Section 3.3.4 below), would be accepted, however, further provision of surface SuDS, with a preference for above ground treatment in the form of swales should be incorporated to aid biodiversity. This request has been implemented with a dedicated drawing created which now identifies the location of all SuDS devices shown, as per drawing number: 18-091-P235.

Flow Control:

A flow control device (Hydrobrake or similar approved) is proposed at each sub-catchment attenuation feature, which will limit exiting flows to the greenfield equivalent runoff rate.

Attenuation tanks:

Attenuation tanks/systems are proposed to be utilised for all catchments within the development as discussed above. Each attenuation tank/system has been sized to accommodate attenuation from catchments for rainfall events greater than the 1-in-100-year event.

Please refer to Appendix D for attenuation calculations for each catchment.

The proposed attenuation tanks/systems to serve the apartment blocks (refer to catchments 2 & 4, in *Table 6*), will be located in areas to remain under private management, and will be privately maintained as such.

Petrol interceptor:

Class 1 petrol interceptors will be provided before the surface water outfalls to the local water courses.

3.4 Interception or Treatment Storage and Attenuation Storage

As noted above, the methodology involved in developing the Storm Water Management Plan for the subject site is based on recommendations set out in the Greater Dublin Strategic Drainage Study (GDSDS) and in the SuDS Manual. Appendix E of the Greater Dublin Strategic Drainage Study (GDSDS) sets out criteria for determining the provision of interception or treatment storage, attenuation storage and long-term storage at a development site. These calculations are summarised below:

3.4.1 Criterion 1: River Water Quality Protection

Criterion 1.1: Interception

The Greater Dublin Strategic Drainage Study (GDSDS) states that approximately 30% to 40% of rainfall events are sufficiently small that there is no measurable runoff from greenfield areas into the receiving waters. These events are generally considered as the first 5mm of rainfall. Assuming 80% runoff from paved surfaces and 0% from pervious surfaces for the first 5mm of rainfall yields the following:

Paved surfaces connected to drainage system	$110,448m^2 \times 0.56 \times 0.75 =$ 46,388.16m ²	110,448m ² site area 56% of the site is paved 75% of the paved area
Volume of Interception Storage	$46,388m^2 \times 5mm \times 0.8 =$ 185.55m³	Paved area directly drained 5mm rainfall depth 80% paved runoff factor

Table 4 | Interception Calculation

The required interception volume is 186m³. It is not proposed to provide the entire required interception volume. Criterion 1.2 will therefore be assessed to provide the required River Water Quality Protection in accordance with Criterion 1.

Criterion 1.2: Treatment Volume

For events larger than 5mm, and in situations where interception storage cannot be provided, surface water runoff treatment is provided utilising SuDS in accordance with the CIRIA design manual C521.

Assuming 80% runoff from paved surfaces and 0% from pervious surfaces for the first 15mm of rainfall:

Paved surfaces draining to river	$110,448m^2 \times 0.56 \times 0.75 =$ 46,388.16m ²	110,448m ² site area 51% of the site is paved 75% of the paved area
Volume of Treatment Storage	$46,388m^2 \times 15mm \times 0.8 =$ 556.66m³	Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces

Table 5 | Treatment Volume Calculation

The required treatment volume for the site is met through the introduction of various SuDS features (which have been described in Section 3.2, above).

Permeable paving is proposed in private driveways and accounts for a total cumulative area of C. 9,034m². Assuming a subbase depth of 0.4m with 33% voids, this yields a treatment volume of 1,192m³.

As noted above, the green sedum roofing amounts to a cumulative area of approximately 1,949m² and shall consist of 75mm substrate with a sedum blanket. Assuming a 30% water volume retention, this amounts to approximately 44m³ of treatment storage volume. Filter drains, swales, raingardens, and roadside trees around the site provide further treatment volume.

These SuDS features provide ample treatment volume to meet the Criteria 1 requirements.

3.4.2 Criterion 2: River Regime Protection

Attenuation storage is provided to limit the discharge rate from the site into receiving waters. As per the GDSDS, the required attenuation volume is calculated assuming 80% runoff from paved areas (20% assumed as permeable paved parking bays, excludes calculations for apartment blocks which have been calculated as 100%), and has been calculated for the 1-year, 30-year and 100-year return periods, identifying the critical storm for each – refer to calculations included in Appendix D.

The calculations included in Appendix D have been based on the usage of soil type 4, as specified by Item 3 of the Surface Water section of the Fingal County Council Water Services Department Report, included as an appendix to the Fingal Planning Authority, Written Opinion Report. Utilising Soil Type 4 for attenuation calculations is also in-line with the data received from the Site Investigation Reports, which note the soil as generally having low permeability. This is reflected in the Site Investigation reports which notes an impermeable brown boulder clay throughout the site. See the Site Investigation reports accompanying report 18-081r.003.

As noted above, the site has been divided into eight sub-catchments which will be attenuated separately. Based on the calculations, included as Appendix D, the required attenuation storage volume for each sub-catchment is set out in *Table 6* below.

Catchment	Area	Allowable Discharge Rate	Required Attenuation Volume
	m^2	/s	m^3
Catchment 1: North 1	13,481	9.00	171.4
Catchment 2: Block C	646	2	14.8
Catchment 3: North 2	15,684	10.47	439.6
Catchment 4: Blocks A & B	4,126	2.75	182.3
Catchment 5: North 3	27,907	18.62	482.2
Catchment 6: North 4	19,827	13.23	319.7
Catchment 7: South 1	9,584	6.40	143.6
Catchment 8: South 2	19,193	12.81	280.4
Total	110,448	75.28	2,034

Table 6 | Attenuation Volume for Each Sub-Catchment

The catchments will be attenuated in individual underground attenuation tanks, with some of the tanks located on the northern site running in a chain-like system. The proposed attenuation tanks will normally remain dry except in extreme weather events and will have a combined storm water storage capacity of 2,034m³ minimum. This provides sufficient storage to accommodate the 1-in-100-year storm volume, accounting for a 20% increase due to climate change. Water will discharge from the tanks to the adjacent existing natural surface water networks via a Hydrobrake or similar approved flow control device at a controlled discharge rate limited to greenfield rates, as shown in the allowable discharge rate column of *Table 6*, above.

Catchments 2 & 4, which are comprised of apartment blocks are intended to have their tanks located in areas which will remain under private management, and as such, the tanks will be privately maintained.

3.4.3 Criterion 3: Levels of Service

There are four criteria for levels of service. These are:

- Criterion 3.1: No external flooding except where specifically planned (30-year high intensity rainfall event).

- Criterion 3.2: No internal flooding (100-year high intensity rainfall event).
- Criterion 3.3: No internal flooding (100-year river event and critical duration for site storage).
- Criterion 3.4: No flood routing off site except where specifically planned (100-year high intensity rainfall event).

Both internal and external flooding have been assessed in the Flood Risk Assessment report which accompanies this Engineering Assessment report. The Flood Risk Assessment has been carried out in accordance with the *DEHLG/OPW Guidelines on the Planning Process and Flood Risk Management* published in November 2009.

The assessment identifies the risk of both internal and external flooding at the site from various sources and sets out mitigation measures against the potential risks of flooding. The sources of possible flooding assessed in the report include coastal, fluvial, pluvial (direct heavy rain), groundwater and human/mechanical errors.

As a result of the flood risk management and mitigation measures proposed, the residual risk of internal or external flooding for the 30-year and 100-year flood events is low, and accordingly all four of the above criteria have been met. Please refer to the accompanying Flood Risk Assessment report for the full analysis of the flood risk at the subject site.

3.4.4 Criterion 4: River Flood Protection

The long-term storage volume is a comparison of pre- and post-development runoff volumes. The objective is to limit the runoff discharged after development to the same as that which occurred prior to development.

Of the three methods described in the GDSDS for establishing River Flood Protection by comparison of the pre- and post-development runoff volumes, (Criteria 4.1, 4.2 and 4.3 respectively), Criteria 4.3 is selected for use as the most practical criteria at this stage in the design.

The Criteria 4.3 approach is for all runoff to be limited to either Q_{BAR} or to 2 l/s/Ha, whichever is the greater. The proposed drainage system includes flow control devices at the outfall for each catchment to ensure that the discharge rate is limited to the greenfield equivalent and ample attenuation is provided for the 1-in-100 year storm, accounting for a 20% increase due to climate change.

The extra runoff volume of the development runoff over greenfield runoff, Vol_{xs} , is calculated in Appendix D for each of the sub-catchments. Note that as stated in the GDSDS, this volume is not additional to the attenuation storage volume but is effectively an element of it.

3.5 Surface Water – General

Surface water sewers will generally consist of PVC (to IS 123) or concrete socket and spigot pipes (to IS 6) and laid strictly in accordance with Fingal County Council requirements for taking in charge. It is intended that all sewers within the public domain will be handed over to Fingal County Council for taking in charge.

All private outfall manholes will be built in accordance with the Greater Dublin Regional Code of Practice for Drainage Works. No private drainage will be located within public areas.

Drains will be laid in accordance with the requirements of the Building Regulations, Technical Guidance Document H.

3.6 Flood Risk Assessment

A site-specific Flood Risk Assessment has been carried out for the proposed development and accompanies this submission under separate cover.

4. Water Supply

4.1 Existing Water Supply

Irish Water records for the surrounding area have been provided by Fingal County Council.

There is an existing 12" Ø watermain located along Back Road.

100mm Ø HDPE spurs have been strategically provided in the sites to the west, Ashwood Hall adjacent to the north site & Hazelbrook adjacent to the south site. These spurs have been constructed in anticipation of servicing this application. The constructed watermain networks in both Hazelbrook and Ashwood Hall have yet to be Taken in Charge by Irish Water.

Irish water as part of the confirmation of feasibility, refer to appendix A, have advised of minor upgrade works required to be undertaken by the applicant to facilitate the proposed development.

4.2 Proposed Water Supply

For the north site, it is proposed to connect to the 150mm Ø watermain in the main access road, just off Back Road. It is also proposed to provide another 2 connections from the Ashwood Hall residential development to the west (both 100mm Ø). The proposed network consists of a 150mm Ø watermain running along the Main Access Roads, with a series of 100mm Ø branches and loops.

Similarly, the southern site is proposed to have 2 watermain connections (both 100mm Ø) to the Hazelbrook residential development on its western boundary.

As discussed in section 4.1 above, the spurs in the adjacent sites have been designed and located in anticipation of these connections from the proposed development. Letters of consent have been obtained from the adjacent development owners permitting these proposed connections. The proposed internal watermain layout, and the existing networks in the adjacent estates can be seen on Drawing numbers 18-091-P301-P306.

As noted in Section 2.2 above, a revised pre-connection enquiry was submitted to Irish Water; the response letter from Irish Water dated 12 June 2020 is included in Appendix A. In this letter, Irish Water states that a new connection to the existing network is feasible with some local upgrades. The local infrastructural upgrades required are: Approximately 395m of 6" CL to 200mm MDPE in Back Road, approximately 270m of 4" AC to 200mm MDPE in Back Road, and approximately 170m of 100mm uPVC to 160mm MDPE in Ashwood Hall Lane. These works will be agreed with Irish Water as part of the Connection Agreement, prior to commencement of the development.

A Statement of Design Acceptance from Irish water is provided in Appendix B.

4.3 Water Supply Calculations

The calculated water demand at the subject development is set out in the table overleaf. The average domestic demand has been established based on an average occupancy ratio of 2.7 persons per dwelling with a daily domestic per capita consumption of 150 litres per head per day and with a 10% allowance factor. The average day/peak week demand has been taken as 1.25 times the average daily domestic demand, while the peak demand has been taken as 5 times the average day/peak week demand, as per Section 3.7.2 of the Irish Water Code of Practice for Water Infrastructure.

The consumption demand of the creche facility is based on the outflow figure of 90 litres per head per day as per *Table 2*.

Description	Total Population	Water Demand	Average Demand	Average Peak Demand	Peak Demand
	No. People	l/day	l/s	l/s	l/s
252 Houses	680.4	112,266	1.299	1.624	8.120
28 Duplexes	75.6	12,474	0.144	0.180	0.900
135 Apartments	364.5	60,142.5	0.696	0.870	4.350
Creche	100	9,900	0.115	0.144	0.720
Total	1,220.5	194,782.5	2.254	2.818	14.090

Table 7 | Calculation of Water Demand for the Development

The average demand for the development is 2.254 l/s, with a peak demand of 14.090 l/s.

4.4 Water Supply – General

All watermains will be laid strictly in accordance with Irish Water requirements for taking in charge.

Valves, hydrants, scour and sluice valves, and bulk water meters will be provided in accordance with the requirements of Irish Water.

5. Roads and Transport Network

This section provides an overview of the existing and proposed road and transportation network in the vicinity of the site. A comprehensive Traffic and Transport Assessment and Travel Plan have been prepared by Waterman Moylan in accordance with the requirements of the Traffic and Transport Assessment Guidelines published by National Roads Authority in May 2014 and accompanies this submission under separate covers.

5.1 Existing Road Layout

Back Road is located to the north of the subject site, immediately north of Ashwood, and Kinsealy Lane is located to the west of the subject site, immediately west of Castleway and Hazelbrook.

Back Road is a 2-lane carriageway with pedestrian footpaths on both sides, it has a posted speed limit of 60km/hr and extends from the Malahide Road (R107) 1.8km east to the Malahide-Donaghmede Road (R124).

Kinsealy Lane is located to the west of the subject site and runs from the junction of the Back Road, south to the junction of Chapel Lane. It has a posted speed limit of 60km/hr. It is a 2 lane-carriageway, and has a footpath on at least 1 side of the road for a distance of 1.4km south from its junction with Back Road, to the entrance to the Sleepy Hollow residential development.

5.2 Proposed Road Layout

The site will be accessed to the north off back Road, via Ashwood.

As requested by Fingal County Council during the SHD pre-planning process, an additional vehicular access to the site is now proposed from Kinsealy Lane, via Hazelbrook. Hazelbrook lies to the west of the proposed southern site. The Hazelbrook development is accessed from Kinsealy Lane and was designed and constructed to allow for possible future connections to the subject site. This will benefit the southern site for vehicular, pedestrian and cycle access. It is considered that the route between the site entrance from the Hazelbrook residential development to the site entrance on Back Road, and vice versa, will not create a short-cut / “rat-run” if there is any potential build-up of traffic at the Kinsealy Lane-Back Road junction. This is owing to the fact the layout of the route through the proposed development is meandering, and has frequent interruptions such; as raised tables, pedestrian crossings and low radii corners which will effectively enforce a slower vehicular speed as per DMURS guidelines. Footpath widths are 2m minimum throughout, with carriageway widths generally between 5-5.5m wide. Horizontal and vertical deflections have been introduced to reduce vehicular speeds, and a swept path and sightlines analysis have been undertaken. Full DMURS details are included in the DMURS report submitted under a separate cover.

A redesign of the creche drop-off parking was also undertaken based on details discussed with Fingal County Council. The creche drop off spaces are located on the same side of the road as the creche, the parking bays are parallel, and a buffer strip has been provided between the bays and carriageway. A circulatory route has been provided for cars to exit the development via the same entrance point, so as to ensure that no 3-point turns are required.

The internal road network includes local access roads and “home-zones”, as shown on Waterman Moylan’s Road Surfacing Layout Drawing 18-091-P002. These homezones have been refined following guidance from An Bord Pleanála and Fingal County Council during the pre-planning process and are further described below in Section 5.3.

The road layout is shown the following drawing numbers: P002 Road Surfacing Layout, Road General Arrangement Drawing P100, Road Layout Drawings P101-103, Road Cross Sections Drawing P130 & Road Construction Details P131, included as part of the planning application package.

Appendices

A. Confirmation of Feasibility Letter - CDS19000369

Stephen Dent-Neville
EastPoint Business Park
Block S, Alfie Byrne Road
Dublin 3, Dublin

13 January 2021

Uisce Éireann
Bosca OP 448
Oifig Sheachadha na
Cathrach Theas
Cathair Chorcal

Irish Water
PO Box 448,
South City
Delivery Office,
Cork City.

www.water.ie

Dear Stephen Dent-Neville,

**Re: Connection Reference No CDS19000369 pre-connection enquiry -
Subject to contract | Contract denied**

Connection for Housing Development of 450 units at Broomfield, Malahide, Dublin.

Irish Water has reviewed your pre-connection enquiry in relation to a water and wastewater connection at Broomfield, Malahide, Dublin.

Based upon the details that you have provided with your pre-connection enquiry and on the capacity currently available in the network(s), as assessed by Irish Water, we wish to advise you that, subject to a valid connection agreement being put in place, your proposed connection to the Irish Water network(s) can be facilitated.

Water

New connection to the existing network is feasible subject to following upgrades:

1. Approximately 395 m of 6" CI to 200 mm MDPE in Back Road
2. Approximately 270 m of 4" AC to 200 mm MDPE in Back Road
3. Approximately 170 m of 100 mm uPVC to 160 mm MDPE in Ashwood Hall Lane

Wastewater

New connection to the network is feasible subject to delivery of the following:

1. Castleway Pumping Station:
 - a) Delivery of a new pumping station to serve the existing and future Connolly Avenue pumping station catchment.
 - b) Procurement of additional lands to facilitate the provision of a total storage volume of 530m3. This includes 362m3 of existing storage at the site. An additional 168m3 storage volume and associated area is required.
 - c) Identification of the required changes to the Malahide discharge licence.
 - d) All environmental (assimilative capacity of receiving water), archaeological and statutory assessments.
 - e) Increase the capacity of Chapel Road Pumping Station currently under construction (Irish Water Capital Investment Plan project) from 53l/s to 94l/s.
 - f) Upgrade of the wastewater gravity network discharging into Castleway Pumping Station.
 - g) Upgrade the wastewater network downstream of Castleway Pumping Station to connect to Chapel Road Pumping Station.
 - h) Provision of Mechanical Electrical and Instrumentation, Control and Automation (MEICA).

- i) Scope of works requirements to incorporate existing MEICA operational requirements (FCC/Irish Water).

Irish Water does not have any plans, in the current Capital Investment Programme (CIP), to undertake these upgrades to facilitate this connection. Should you wish to progress upgrades and associated works, Irish Water may require you to provide a contribution of a relevant portion of the costs for the required upgrades. Engagement with Irish Water will be required to agree the delivery mechanism for the upgrades.

2. Completion of Chapel Road Pumping Station and associated rising main to the North Fringe Sewer (Irish Water CIP - Local Network Reinforcement Project). This Project is currently in progress and scheduled to be completed by Q4 2021 (this may be subject to change).

All infrastructure should be designed and installed in accordance with the Irish Water Codes of Practice and Standard Details. A design proposal for the water and wastewater infrastructure should be submitted to Irish Water for assessment. Prior to submitting your planning application, you are required to submit these detailed design proposals to Irish Water for review.

You are advised that this correspondence does not constitute an offer in whole or in part to provide a connection to any Irish Water infrastructure and is provided subject to a connection agreement being signed at a later date.

A connection agreement can be applied for by completing the connection application form available at www.water.ie/connections. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities.

If you have any further questions, please contact Marina Byrne from the design team via email mzbyrne@water.ie. For further information, visit www.water.ie/connections.

Yours sincerely,



Maria O'Dwyer

Connections and Developer Services

B. Irish Water Statement of Design Acceptance

Richard Wallace
Kinsealy Hall
Chapel Road
Kinsealy, Malahide
Co. Dublin

Uisce Éireann
Bosca OP 448
Oifig Sheachadta na
Cathrach Theas
Cathair Chorcaí

3 February 2022

Irish Water
PO Box 448,
South City
Delivery Office,
Cork City.

www.water.ie

Re: Design Submission for Broomfield, Malahide, Dublin (the “Development”) (the “Design Submission”) / Connection Reference No: CDS19000369

Dear Richard Wallace,

Many thanks for your recent Design Submission.

We have reviewed your proposal for the connection(s) at the Development. Based on the information provided, which included the documents outlined in Appendix A to this letter, Irish Water has no objection to your proposals.

This letter does not constitute an offer, in whole or in part, to provide a connection to any Irish Water infrastructure. Before you can connect to our network you must sign a connection agreement with Irish Water. This can be applied for by completing the connection application form at www.water.ie/connections. Irish Water's current charges for water and wastewater connections are set out in the Water Charges Plan as approved by the Commission for Regulation of Utilities (CRU)(https://www.cru.ie/document_group/irish-waters-water-charges-plan-2018/).

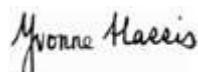
You the Customer (including any designers/contractors or other related parties appointed by you) is entirely responsible for the design and construction of all water and/or wastewater infrastructure within the Development which is necessary to facilitate connection(s) from the boundary of the Development to Irish Water's network(s) (the “**Self-Lay Works**”), as reflected in your Design Submission. Acceptance of the Design Submission by Irish Water does not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.

If you have any further questions, please contact your Irish Water representative:

Name: Dario Alvarez

Email: dalvarez@water.ie

Yours sincerely,



Yvonne Harris

Head of Customer Operations

Appendix A

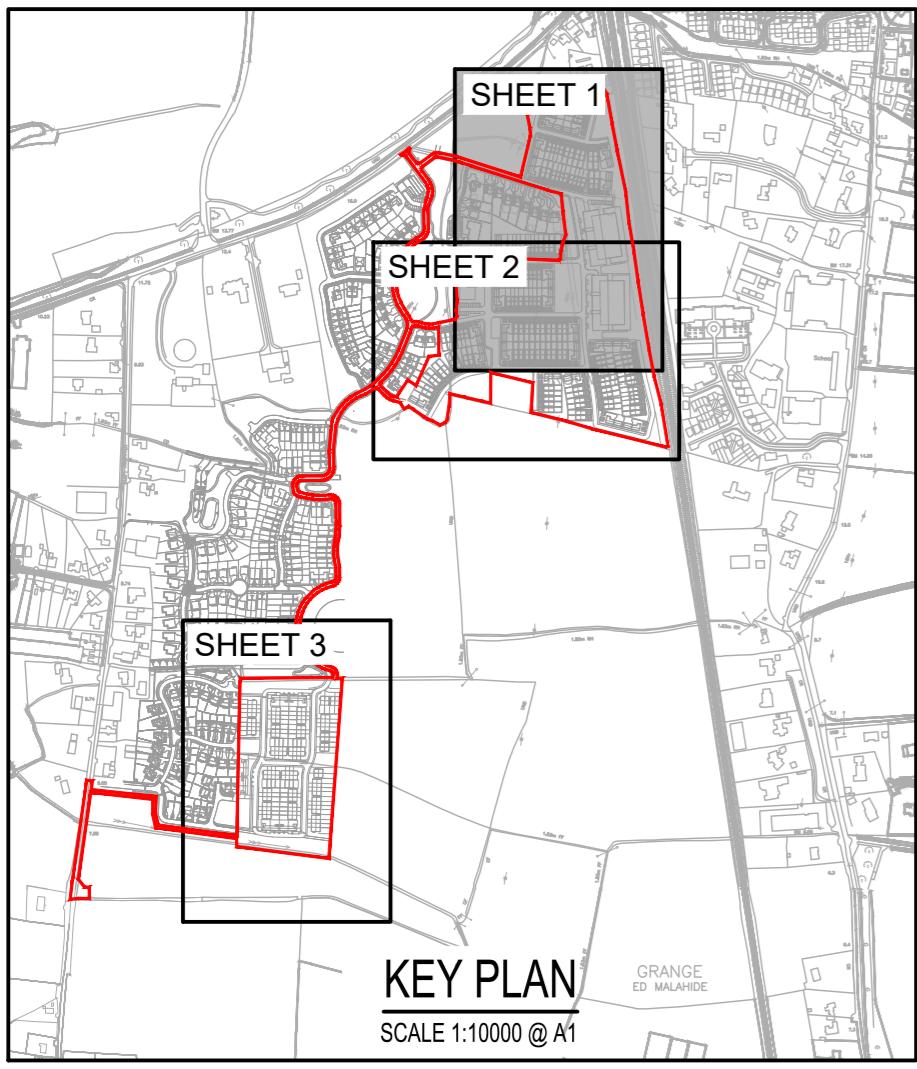
Document Title & Revision

- 18-091-P301A Watermain Layout Sheet 1 of 3
- 18-091-P302A Watermain Layout Sheet 2 of 3
- 18-091-P303A Watermain Layout Sheet 3 of 3
- 18-091-P201A Drainage Layout Sheet 1 of 4
- 18-091-P202A Drainage Layout Sheet 2 of 4
- 18-091-P203A Drainage Layout Sheet 3 of 4
- 18-091-P204A Drainage Layout Sheet 4 of 4
- 18-091-P240 Foul Drainage Longitudinal Sections Sheet 1 of 3
- 18-091-P241 Foul Drainage Longitudinal Sections Sheet 2 of 3
- 18-091-P242 Foul Drainage Longitudinal Sections Sheet 3 of 3

Standard Details/Code of Practice Exemption: N/A

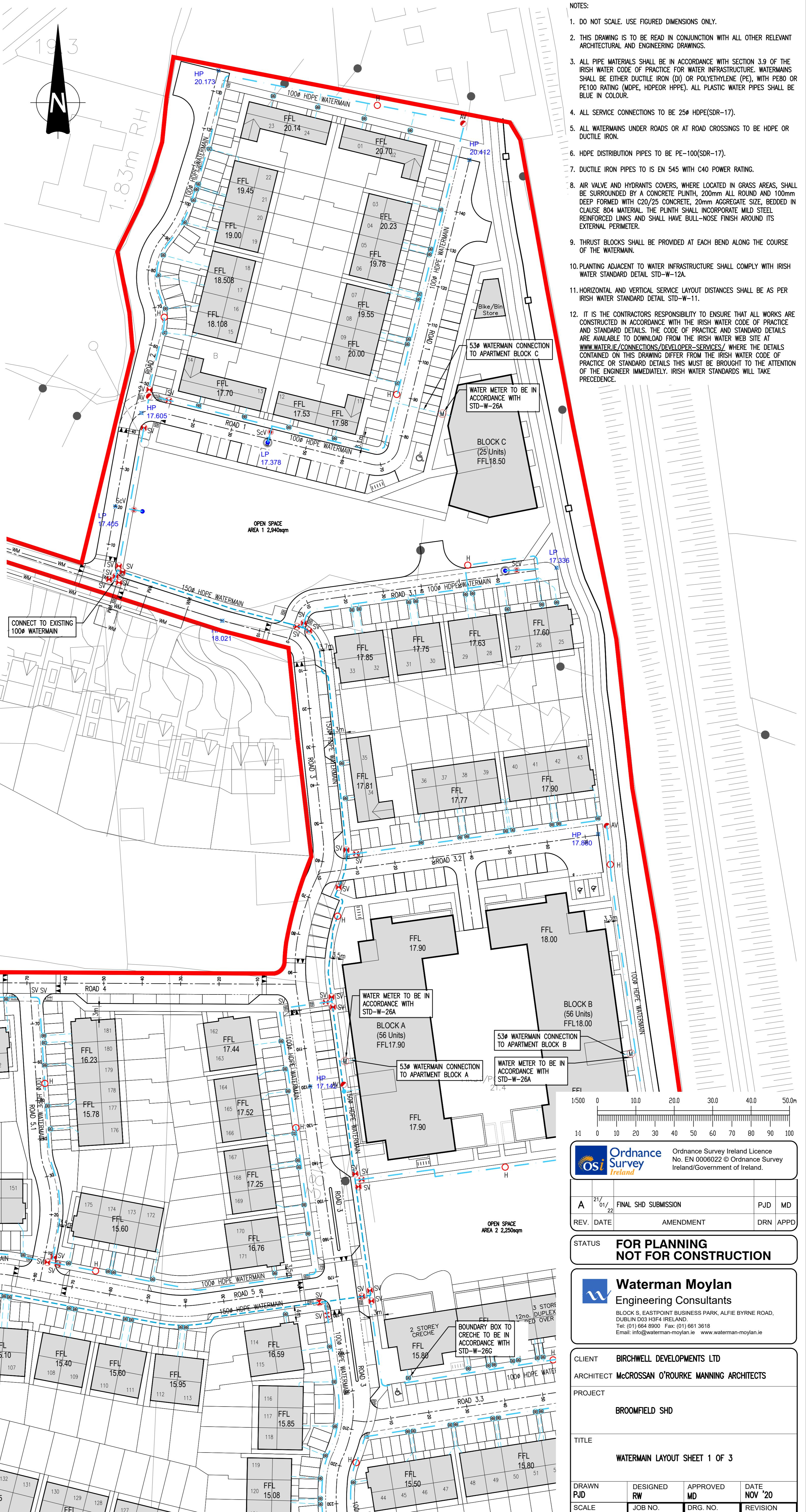
For further information, visit www.water.ie/connections

Notwithstanding any matters listed above, the Customer (including any appointed designers/contractors, etc.) is entirely responsible for the design and construction of the Self-Lay Works. Acceptance of the Design Submission by Irish Water will not, in any way, render Irish Water liable for any elements of the design and/or construction of the Self-Lay Works.



LEGEND:

- XXXXmm Ø PROPOSED 100Ø HDPE WATERMAIN WITH PIPE SIZE
- XXXXmm Ø PROPOSED 150Ø HDPE WATERMAIN WITH PIPE SIZE
- XXXXmm Ø EXISTING WATERMAIN WITH PIPE SIZE
- SV PROPOSED SLUICE VALVE
- H PROPOSED HYDRANT
- ScV PROPOSED SCOUR VALVE
- AV PROPOSED AIR VALVE
- NRV PROPOSED NON-RETURN VALVE
- M PROPOSED BULK WATER METER
- SWMH SURFACE WATER MANHOLE
- WATERMAIN TYPICAL SCHEMATIC CONNECTION OF OFFLINE SCOUR VALVE
- PROPOSED BOUNDARY BOX AND CONNECTION
- LP ROAD LOW POINT
- HP ROAD HIGH POINT



A	21/01/22	FINAL SHD SUBMISSION	PJD	MD
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Waterman Moylan
Engineering Consultants

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DUBLIN D03 H3F4 IRELAND Tel: (01) 664 8900
Email: info@waterman-moylan.ie www.waterman-moylan.ie

CLIENT BIRCHWELL DEVELOPMENTS LTD
ARCHITECT McCROSSAN O'ROURKE MANNING ARCHITECTS
PROJECT BROOMFIELD SHD

TITLE
WATERMAIN LAYOUT SHEET 2 OF 3

DRAWN PJD
DESIGNED RW
APPROVED MD
DATE NOV '20

SCALE 1:500 @ A1
JOB NO. 18-091 DRG. NO. P302 REVISION A

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1:500 0 10.0 20.0 30.0 40.0 50.0m

0 10 20 30 40 50 60 70 80 90 100

WM WM

CONNECT TO EXISTING
100m WATERMAIN

18m LONG & 32°
BOUNDARY BOX CONNECTION

FFL 13.85

OPEN SPACE AREA 3 919sqm

16m LONG & 32°
BOUNDARY BOX CONNECTION

FFL 13.80

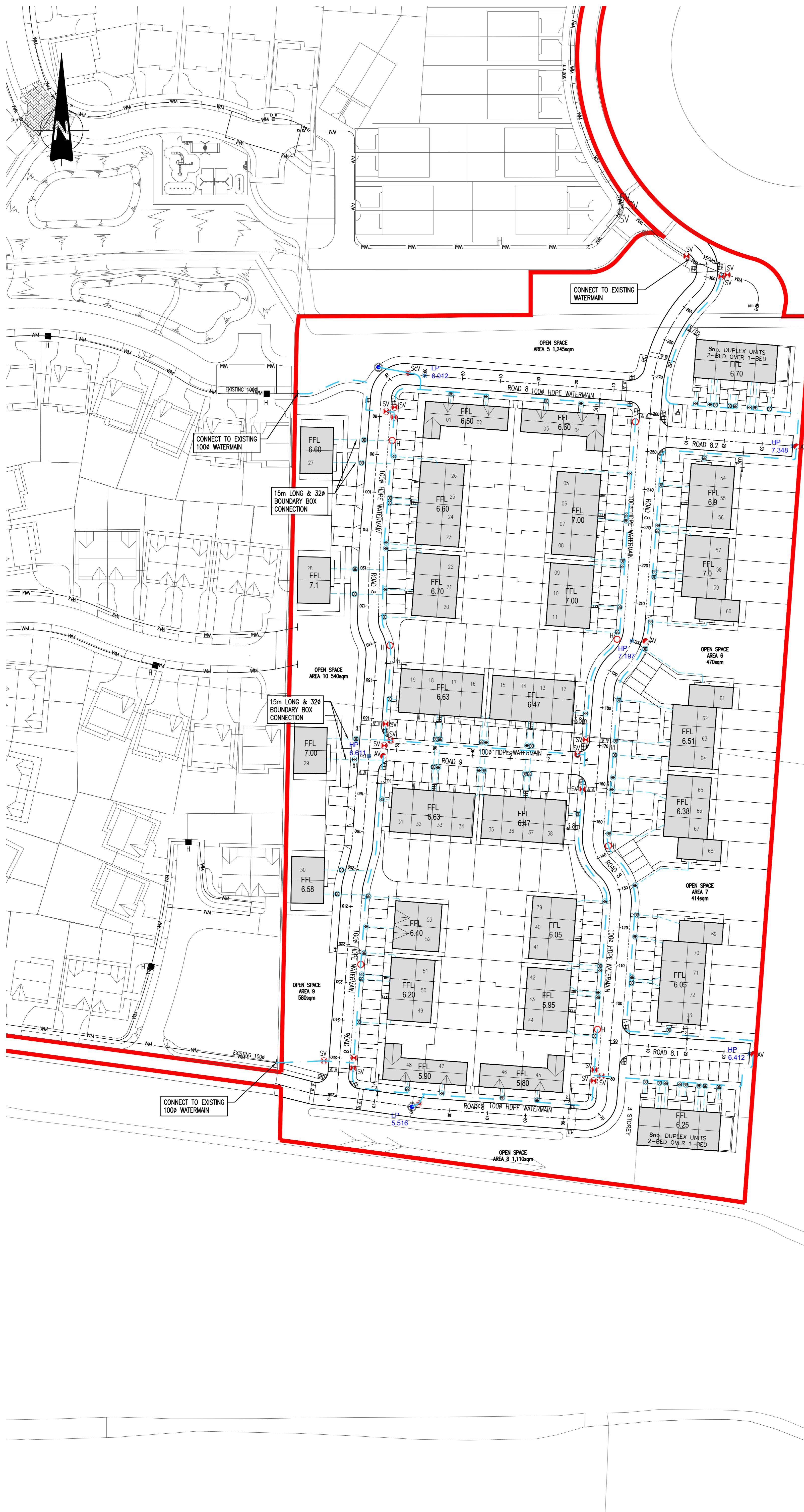
OPEN SPACE AREA 4 2,830sqm

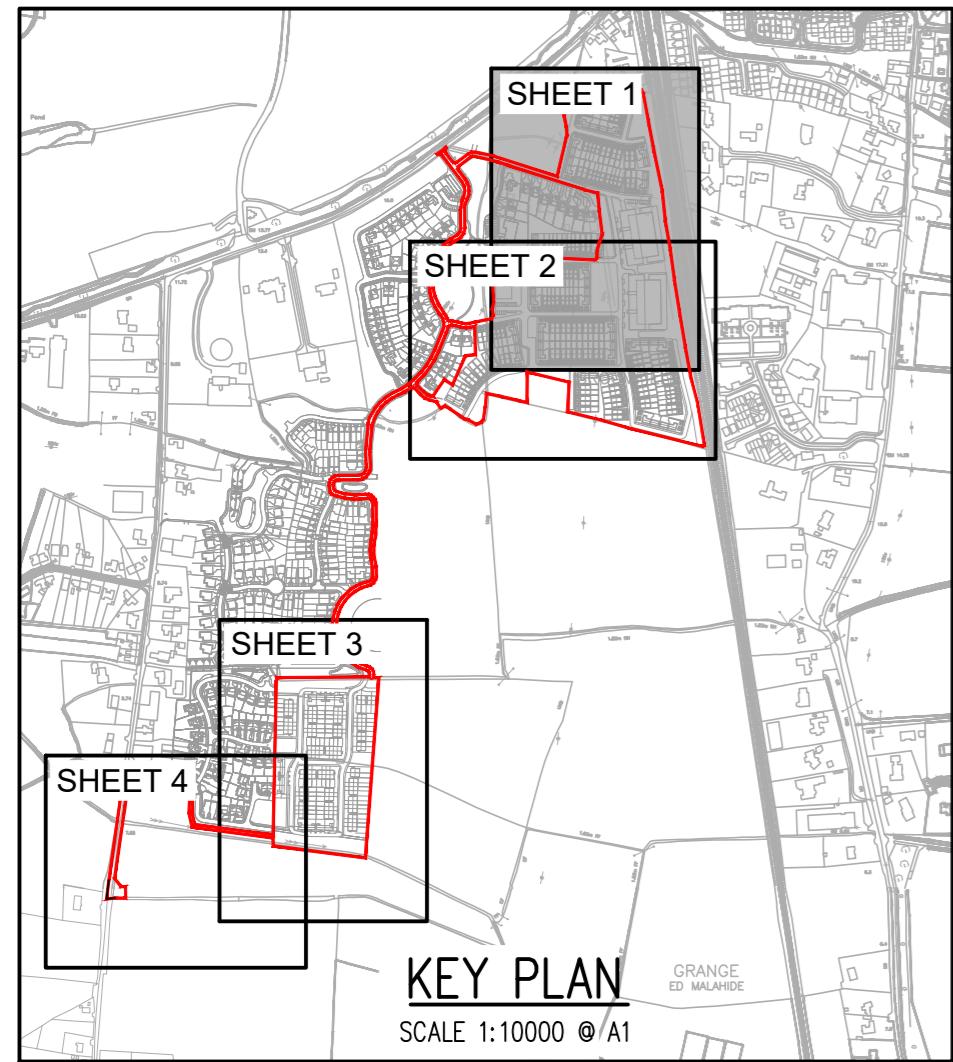
FFL 13.85

150m HDPE WATERMAIN

FFL 13.80

150m HDPE WATERMAIN



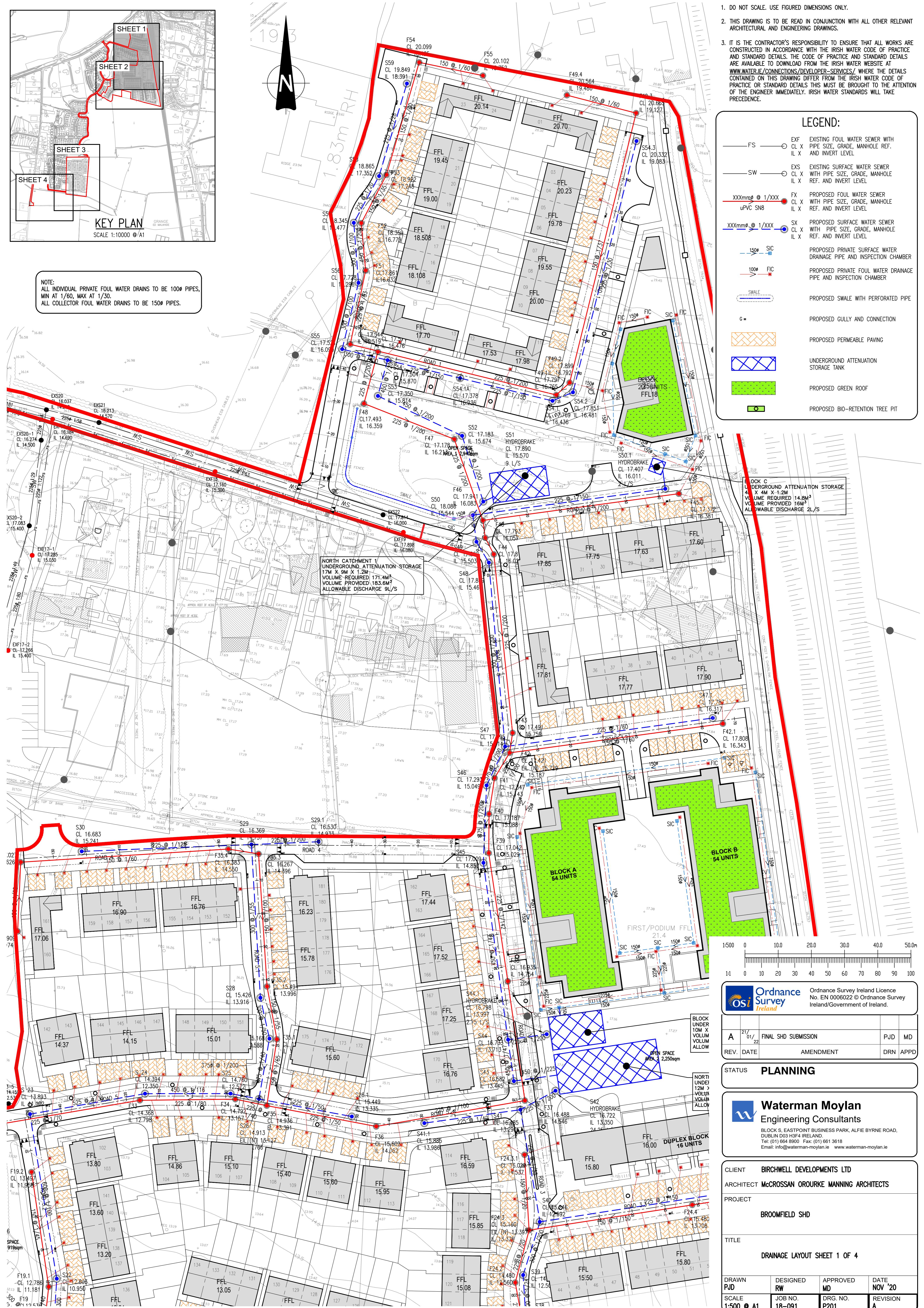


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LEGEND:

	EXF CL X IL X	EXISTING FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
	EXS CL X IL X	EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
	FX CL X IL X	PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
	SX CL X IL X	PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
		PROPOSED PRIVATE SURFACE WATER DRAINAGE PIPE AND INSPECTION CHAMBER
		PROPOSED PRIVATE FOUL WATER DRAINAGE PIPE AND INSPECTION CHAMBER
		PROPOSED SWALE WITH PERFORATED PIPE
		PROPOSED GULLY AND CONNECTION
		PROPOSED PERMEABLE PAVING
		UNDERGROUND ATTENUATION STORAGE TANK
		PROPOSED GREEN ROOF
		PROPOSED BIO-RETENTION TREE PIT

NOTE:
ALL INDIVIDUAL PRIVATE FOUL WATER DRAINS TO BE 100Ø PIPES,
MIN AT 1/60, MAX AT 1/30.
ALL COLLECTOR FOUL WATER DRAINS TO BE 150Ø PIPES.



A 21/01/22 FINAL SHD SUBMISSION PJD MD
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Waterman Moylan
Engineering Consultants

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ARCHITECT McCROSSAN O'ROURKE MANNING ARCHITECTS
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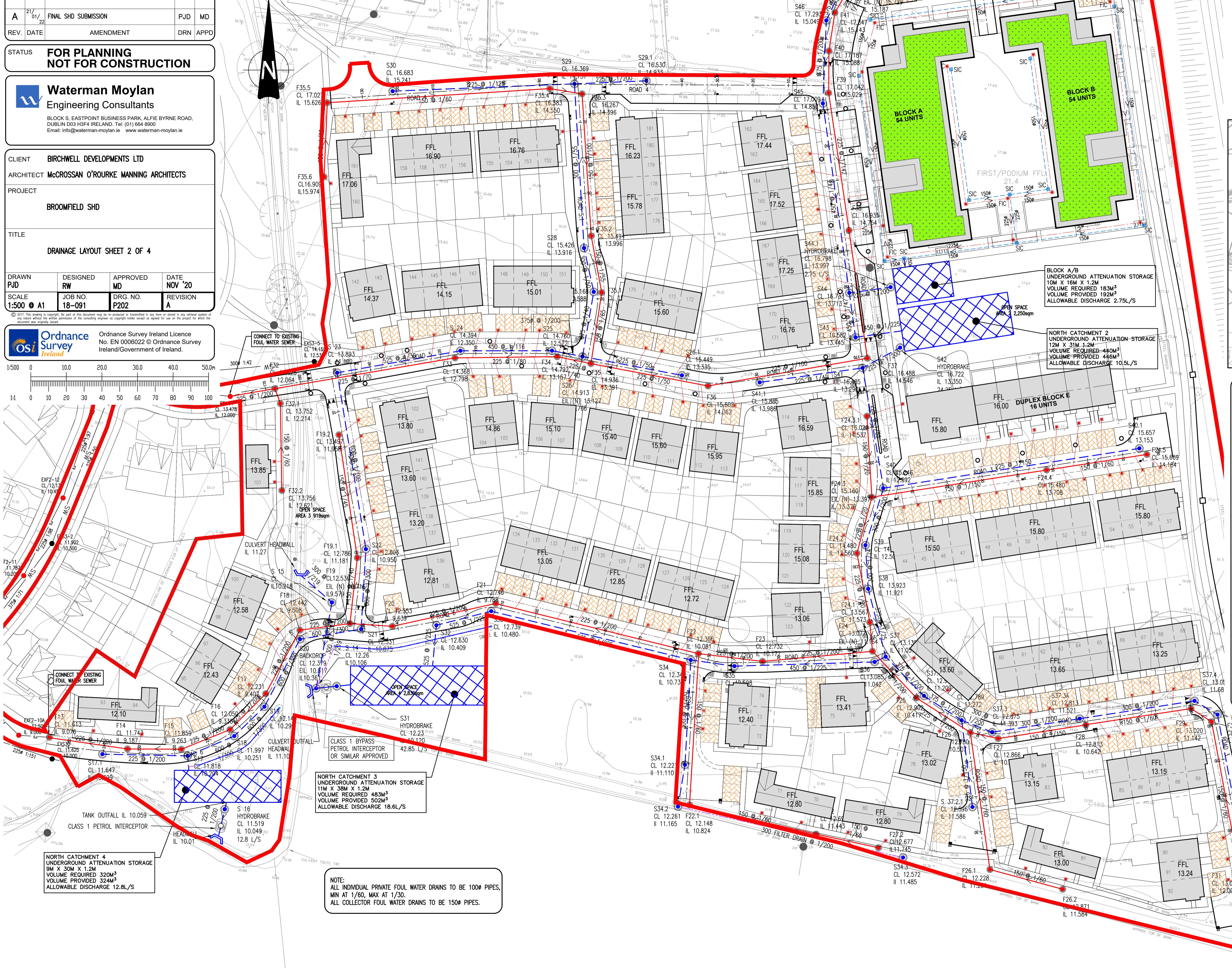
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DRAWN NO. 18-091 DESIGNED NO. P202 APPROVED NO. REVISION A

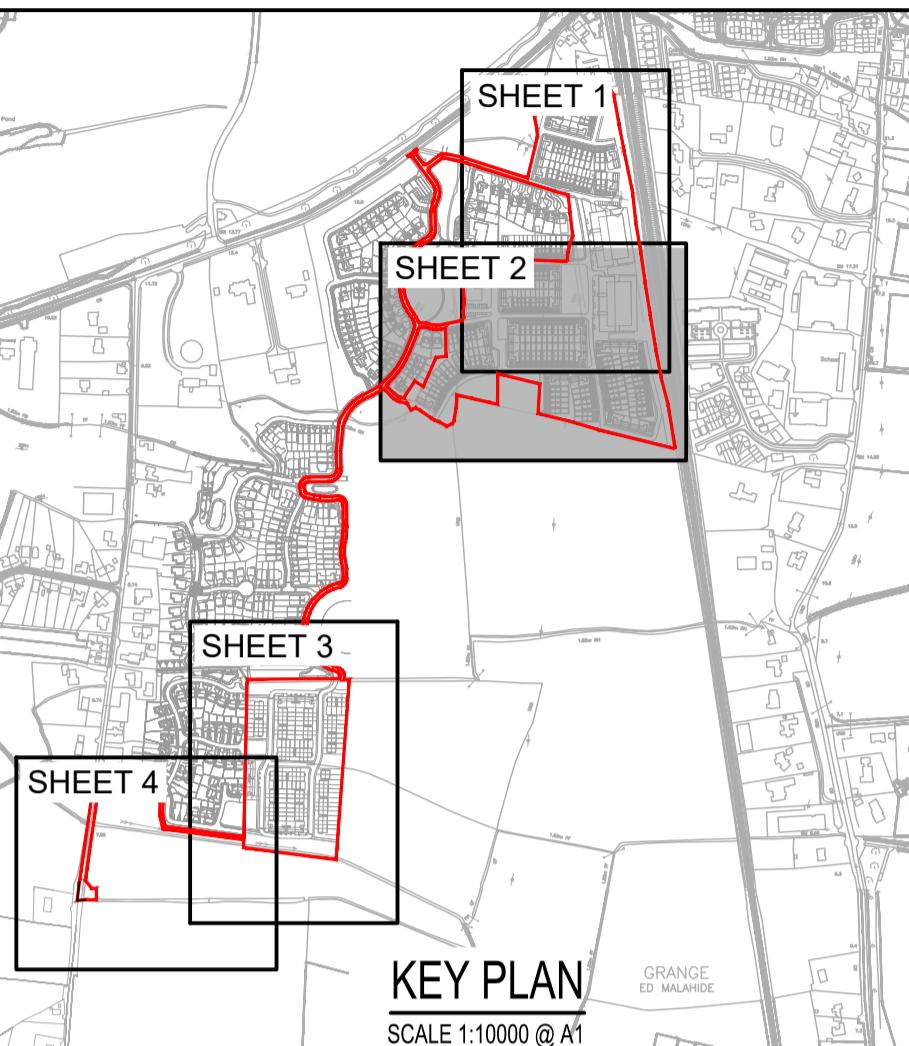
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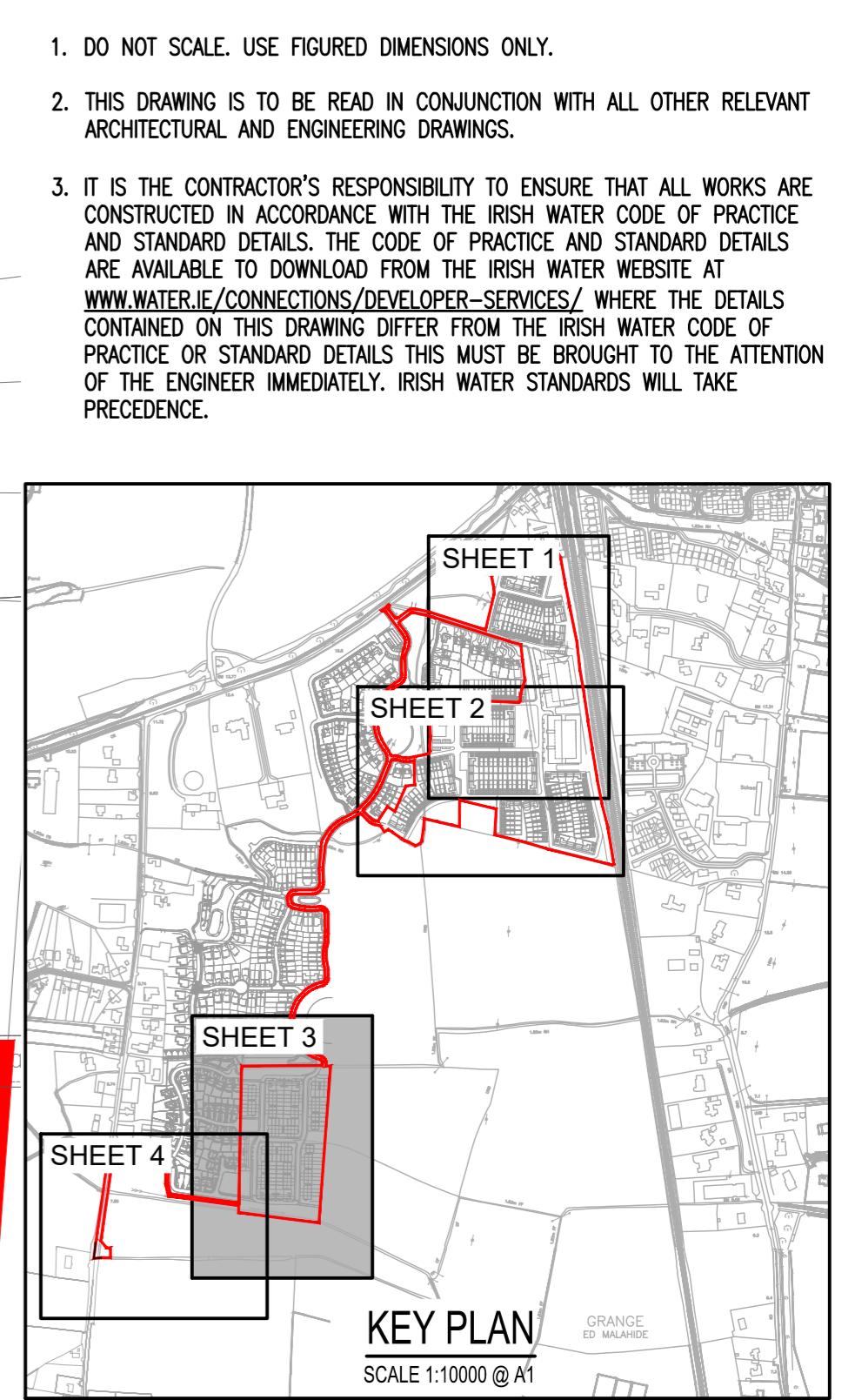
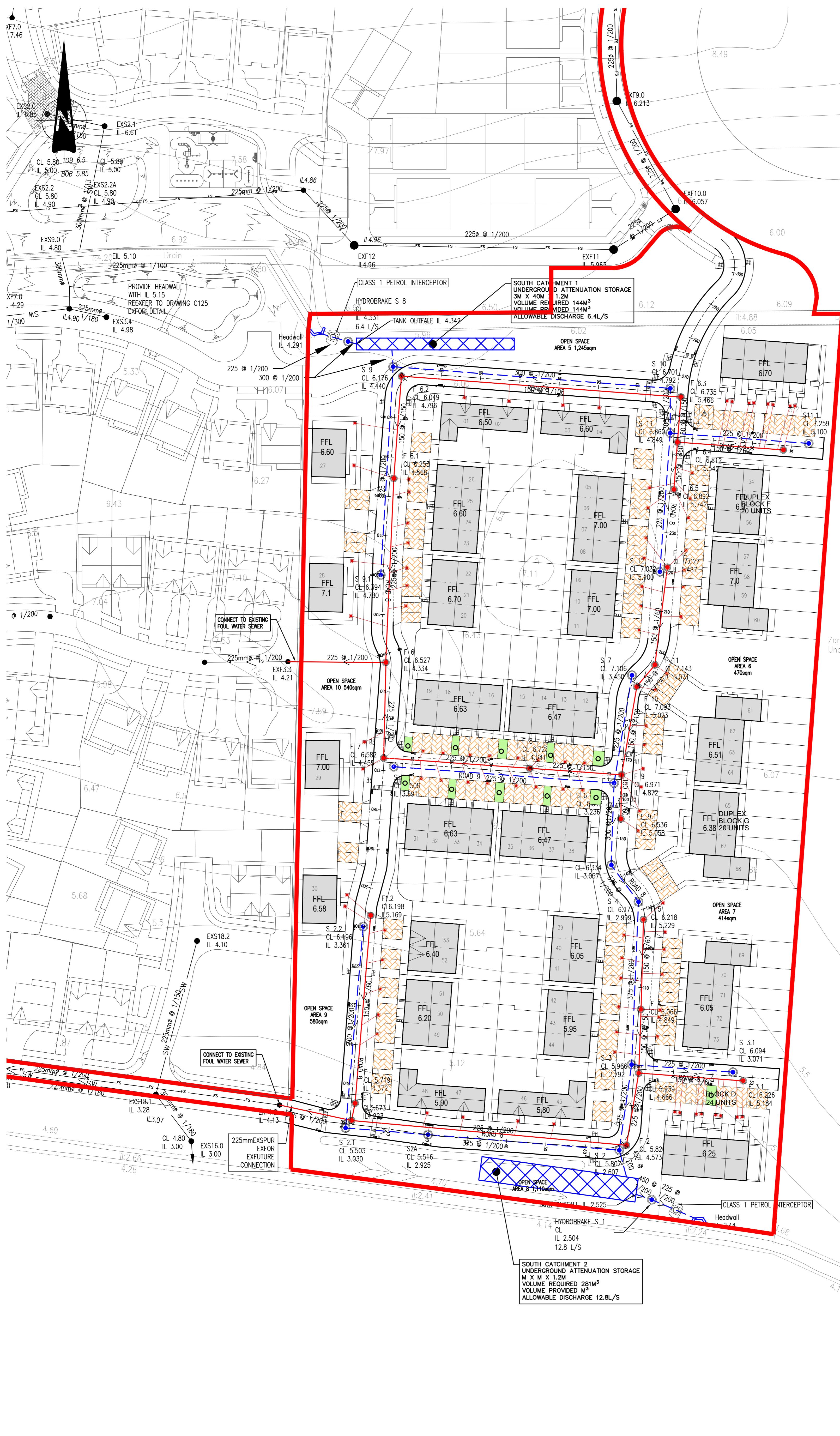


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LEGEND:

FS	EX Foul Water Sewer with Pipe Size, Grade, Manhole Ref. and Invert Level
SW	EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
XXXmm Ø @ 1/XXX	PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
FX	PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
XXXmm Ø @ 1/XXX	PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
150Ø SIC	PROPOSED PRIVATE SURFACE WATER DRAINAGE PIPE AND INSPECTION CHAMBER
100Ø FIC	PROPOSED PRIVATE FOUL WATER DRAINAGE PIPE AND INSPECTION CHAMBER
SWALE	PROPOSED SWALE WITH PERFORATED PIPE
G =	PROPOSED GULLY AND CONNECTION
██████	PROPOSED PERMEABLE PAVING
████████	UNDERGROUND ATTENUATION STORAGE TANK
██████████	PROPOSED GREEN ROOF
███████████	PROPOSED BIO-RETENTION TREE PIT



LEGEND:	
FS	EXS CL X IL X EXISTING FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
SW	EXS CL X IL X EXISTING SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
XXXmm@ 1/XXX	FX CL X IL X PROPOSED FOUL WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
uPVC SNB	
XXXmm@ 1/XXX	SX CL X IL X PROPOSED SURFACE WATER SEWER WITH PIPE SIZE, GRADE, MANHOLE REF. AND INVERT LEVEL
150@ SIC	
100@ FIC	
SWALE	PROPOSED SWALE WITH PERFORATED PIPE
G =	PROPOSED GULLY AND CONNECTION
orange hatching	PROPOSED PERMEABLE PAVING
blue cross-hatching	UNDERGROUND ATTENUATION STORAGE TANK
green dotted pattern	PROPOSED GREEN ROOF
green circle	PROPOSED BIO-RETENTION TREE PIT

NOTE:
ALL INDIVIDUAL PRIVATE FOUL WATER DRAINS TO BE 100@ PIPES,
MIN AT 1/60, MAX AT 1/30.
ALL COLLECTOR FOUL WATER DRAINS TO BE 150@ PIPES.

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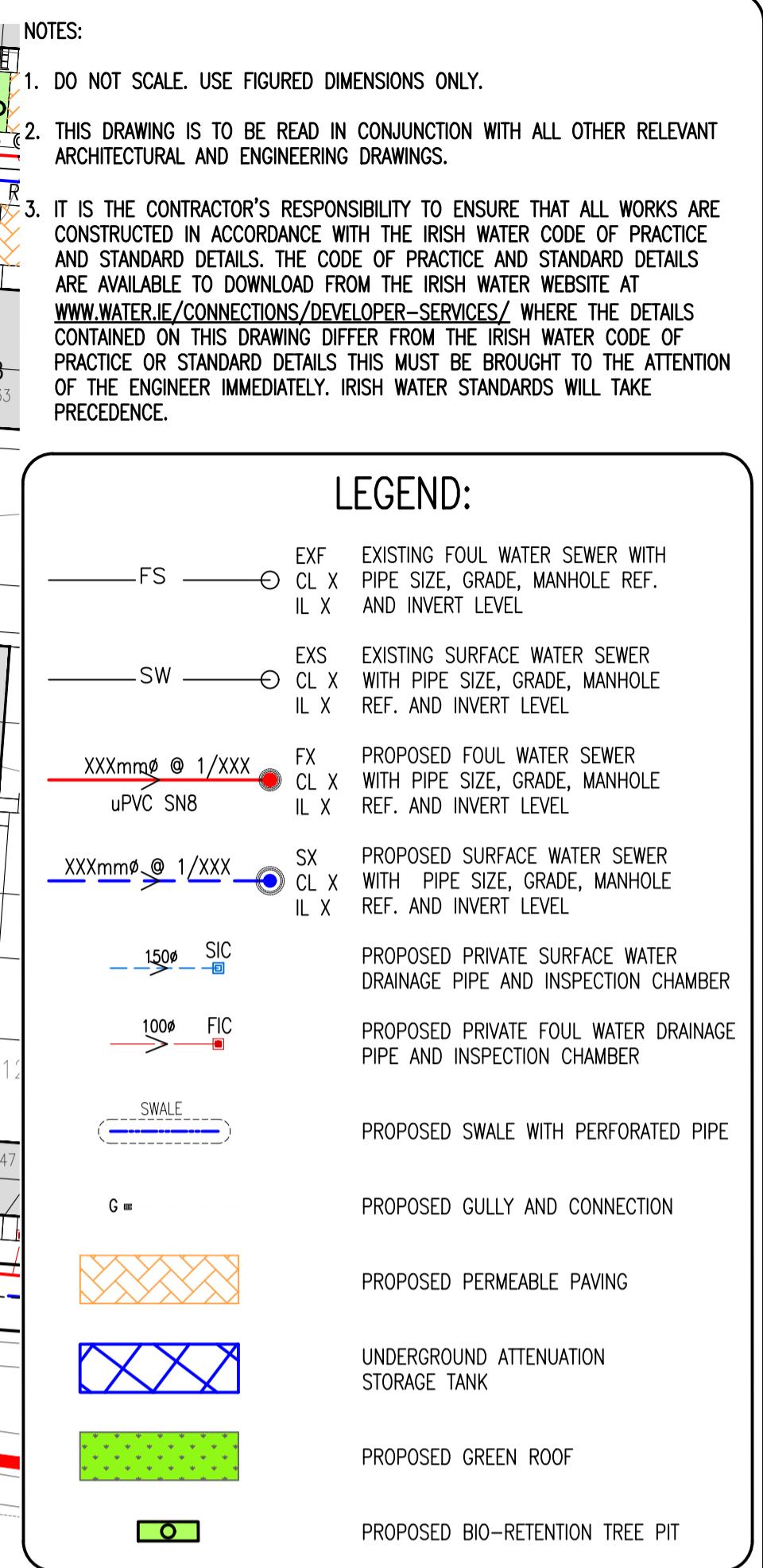
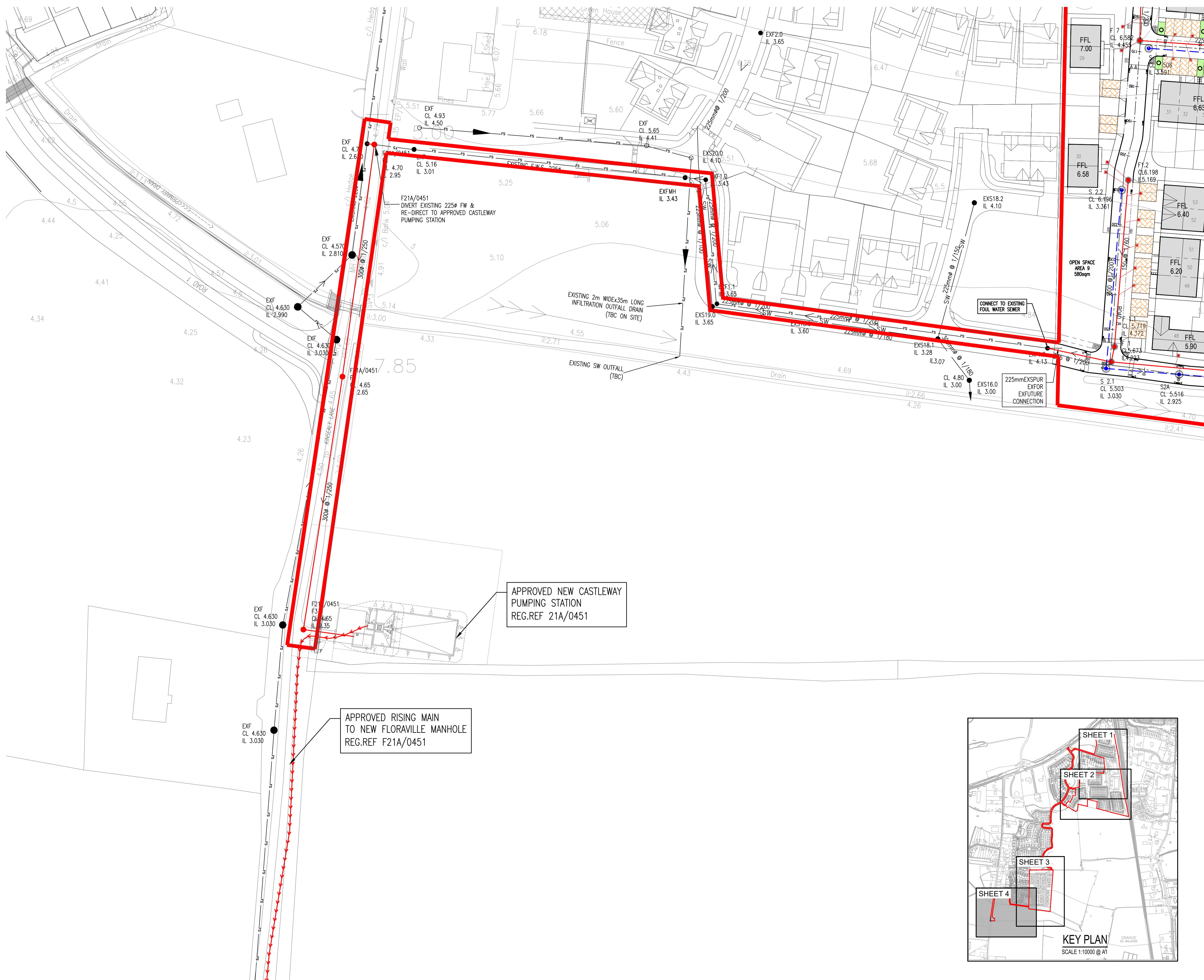
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Engineering Consultants
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DUBLIN D03 H3P4 IRELAND
Tel: (01) 664 8900 Fax: (01) 661 3618
Email: info@waterman-moylan.ie www.waterman-moylan.ie

CLIENT BIRCHWELL DEVELOPMENTS LTD
ARCHITECT McCROSSAN O'ROURKE MANNING ARCHITECTS

PROJECT BROOMFIELD SHD

TITLE DRAINAGE LAYOUT SHEET 3 OF 4

DRAWN PJD	DESIGNED RW	APPROVED MD	DATE NOV '20
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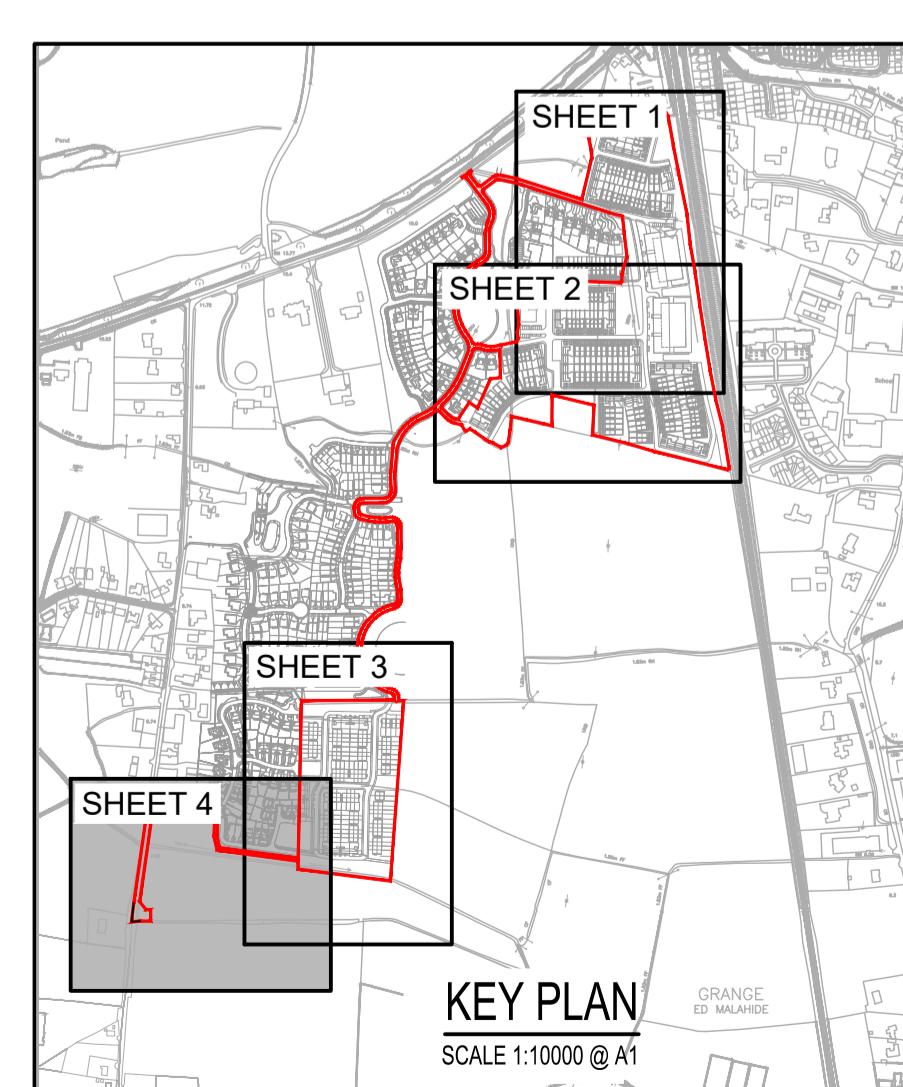
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Waterman Moylan
Engineering Consultants
BLOCK S, EASTPOINT BUSINESS PARK, ALFIE BYRNE ROAD,
DUBLIN D03 H3F4 IRELAND.
Tel: (01) 664 8900 Fax: (01) 661 3618
Email: info@waterman-moylan.ie www.waterman-moylan.ie

CLIENT BIRCHWELL DEVELOPMENTS LTD
ARCHITECT McCROSSAN O'ROURKE MANNING ARCHITECTS
PROJECT BROOMFIELD SHD

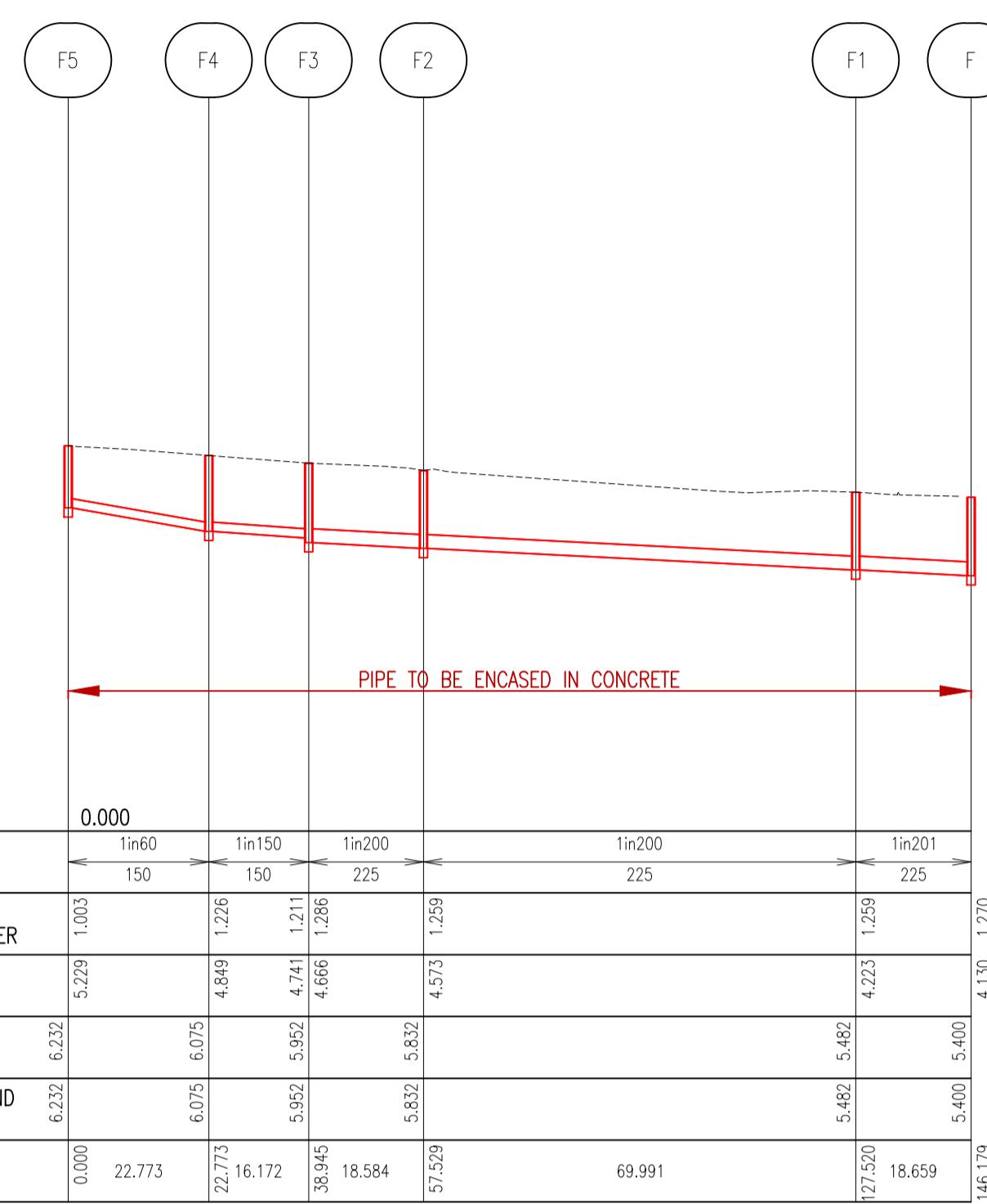
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AS SHOWN @ A1 18-091	JOB NO. DRG. NO.	P204	REVISION A

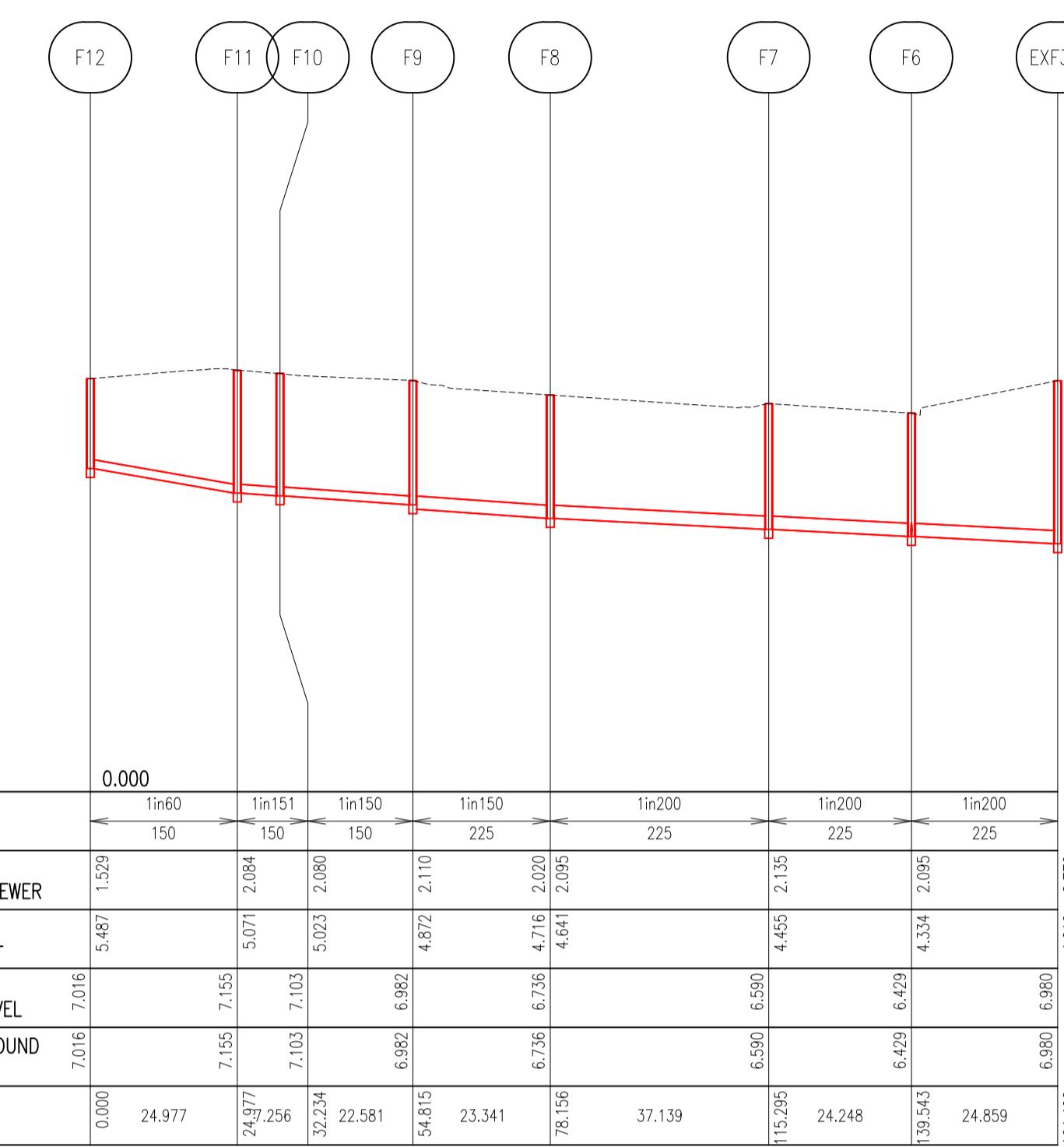


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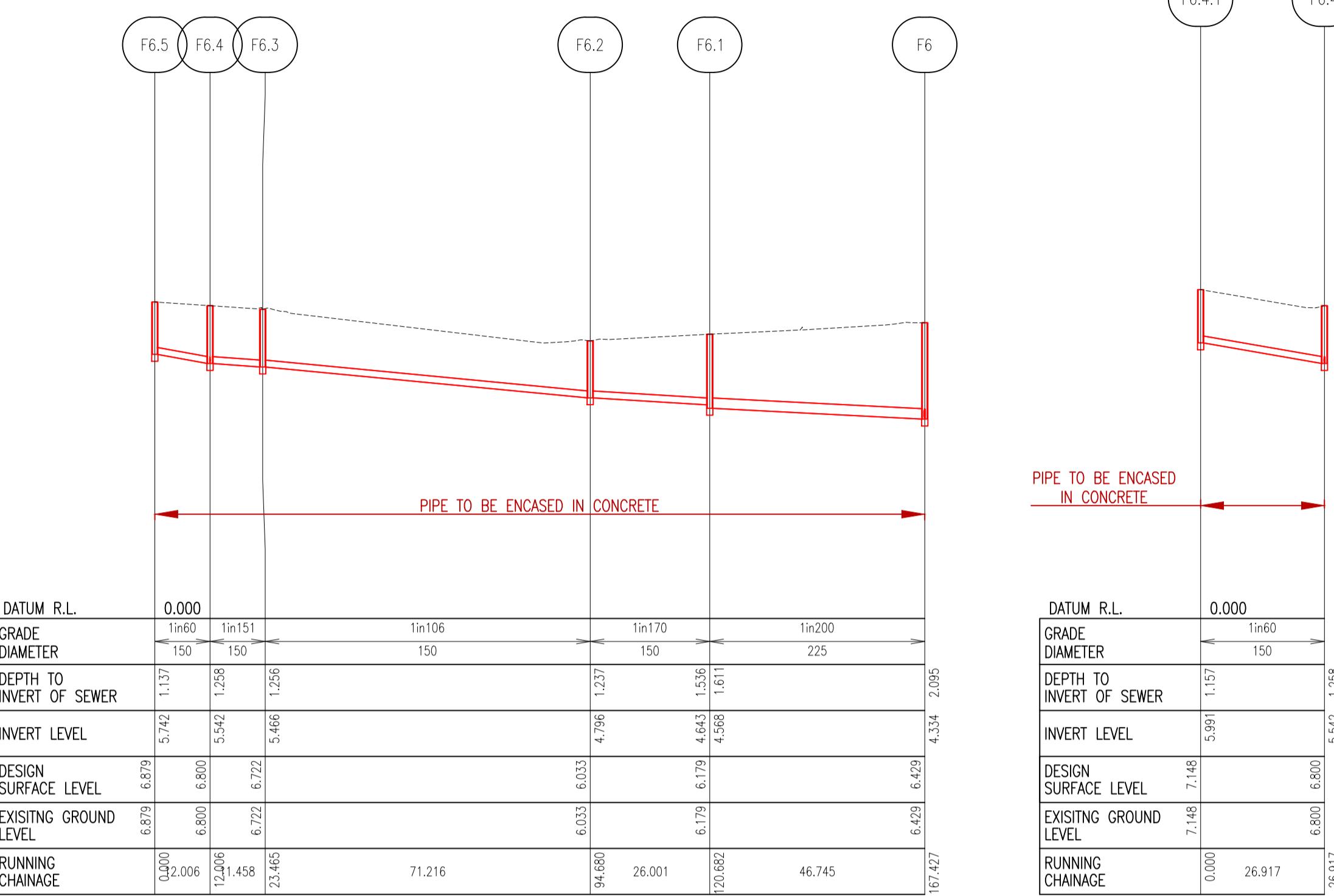
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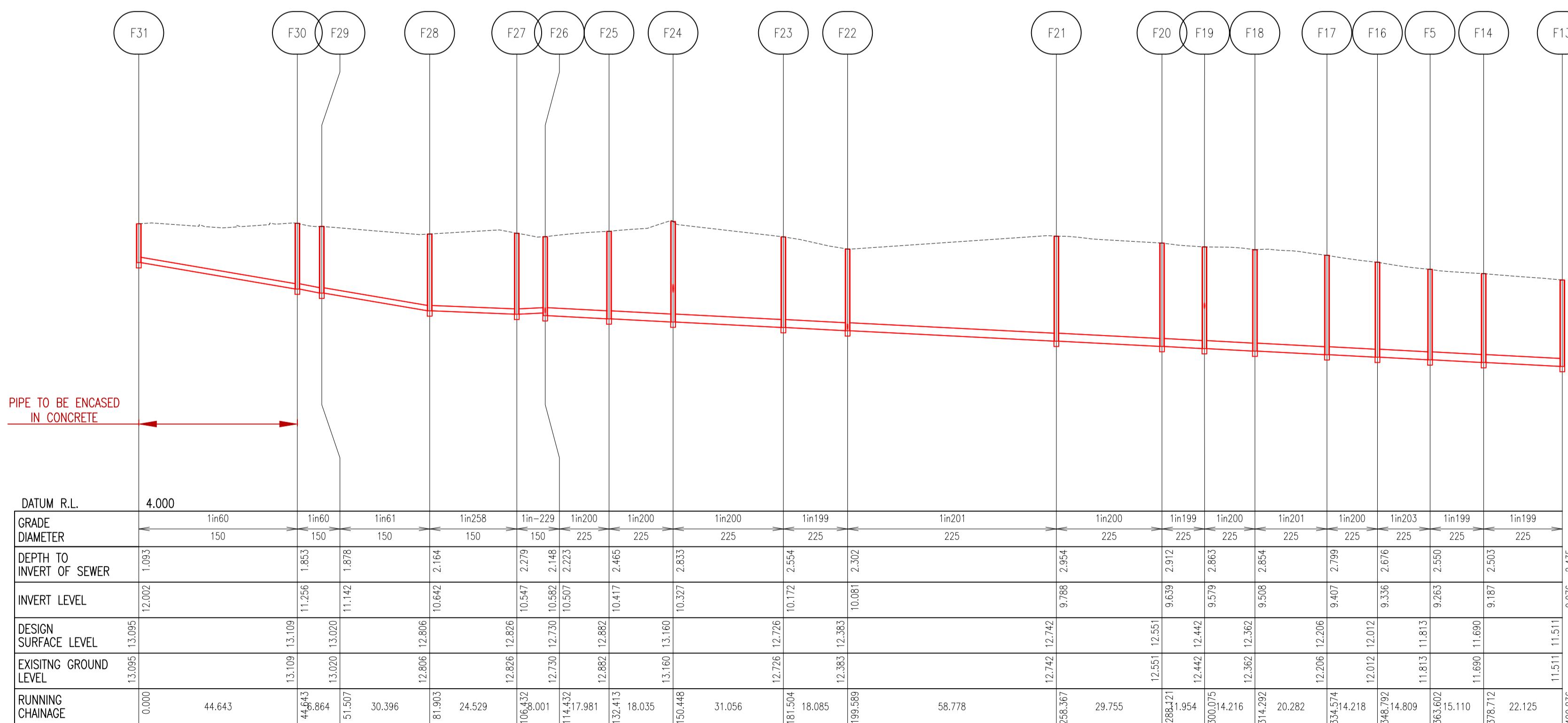
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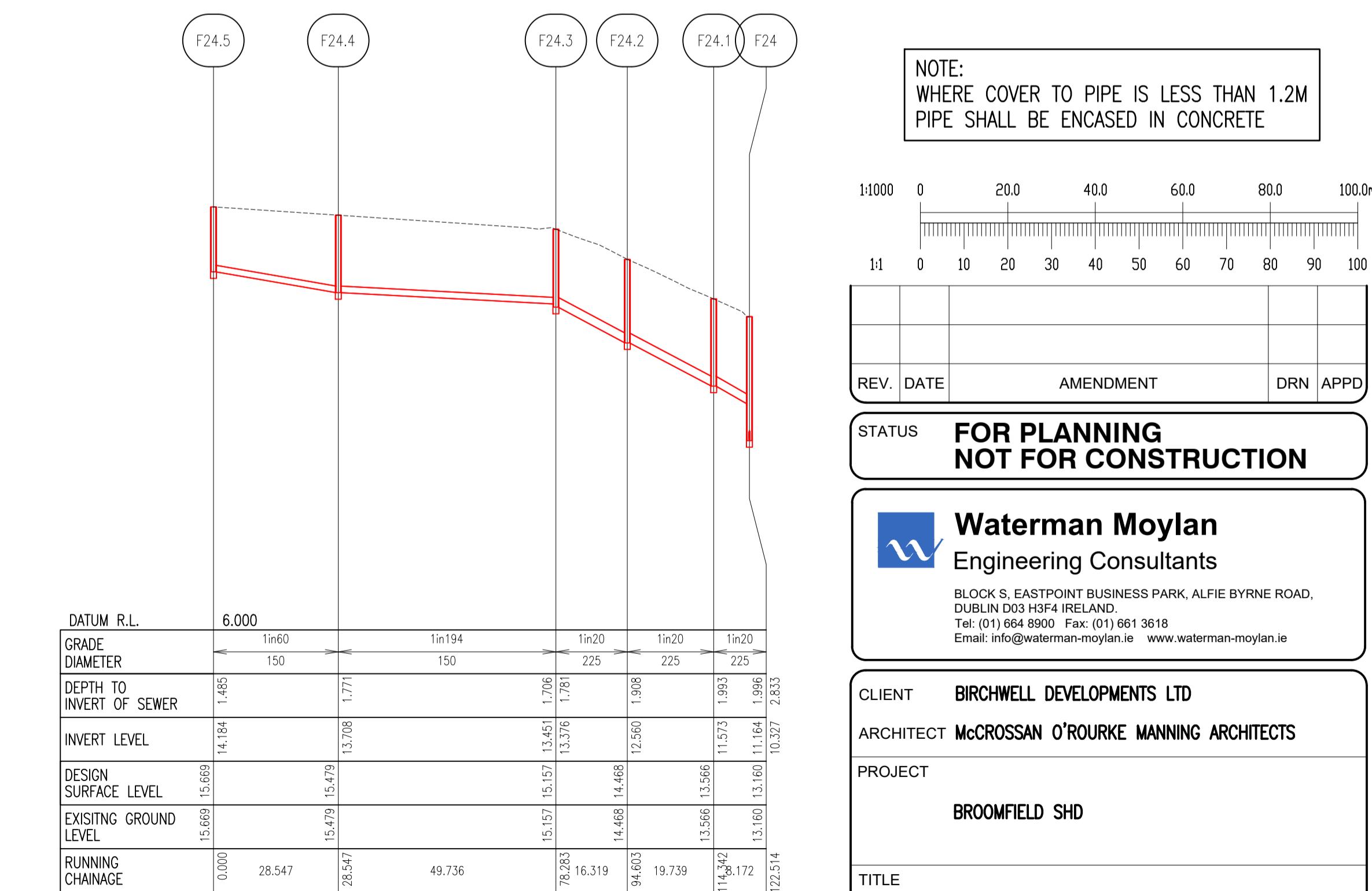
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F005



F007



F008

NOTE:
WHERE COVER TO PIPE IS LESS THAN 1.2M
PIPE SHALL BE ENCASED IN CONCRETE

V.	DATE	AMENDMENT		DRN	APPD			

**FOR PLANNING
NOT FOR CONSTRUCTION**



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WISCONSIN STATEMENT OF READING AND WRITING STANDARDS

BROOMFIELD SHD

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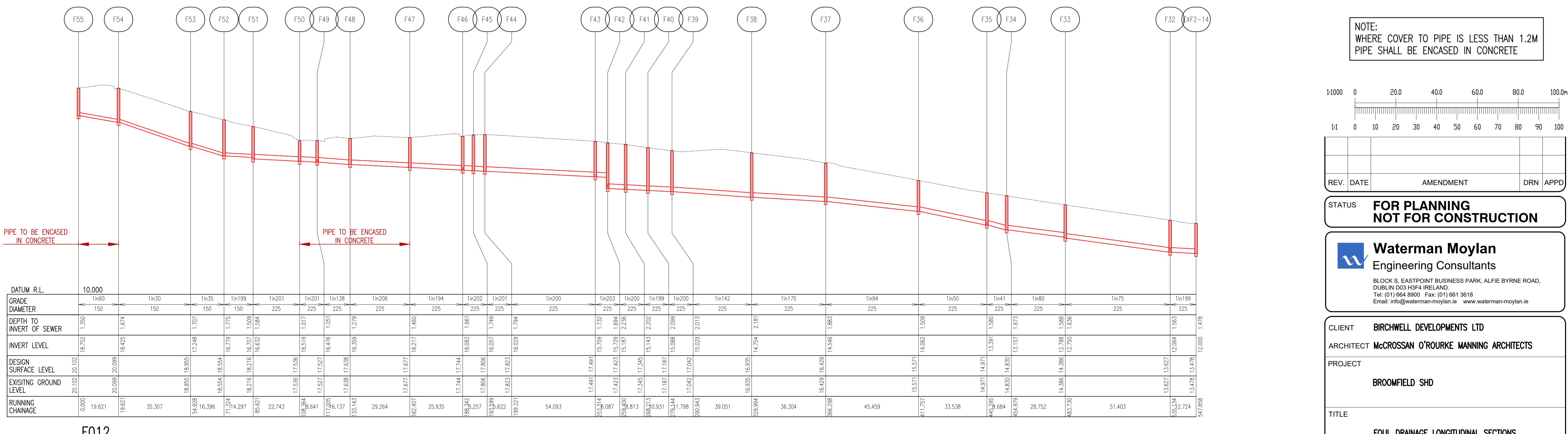
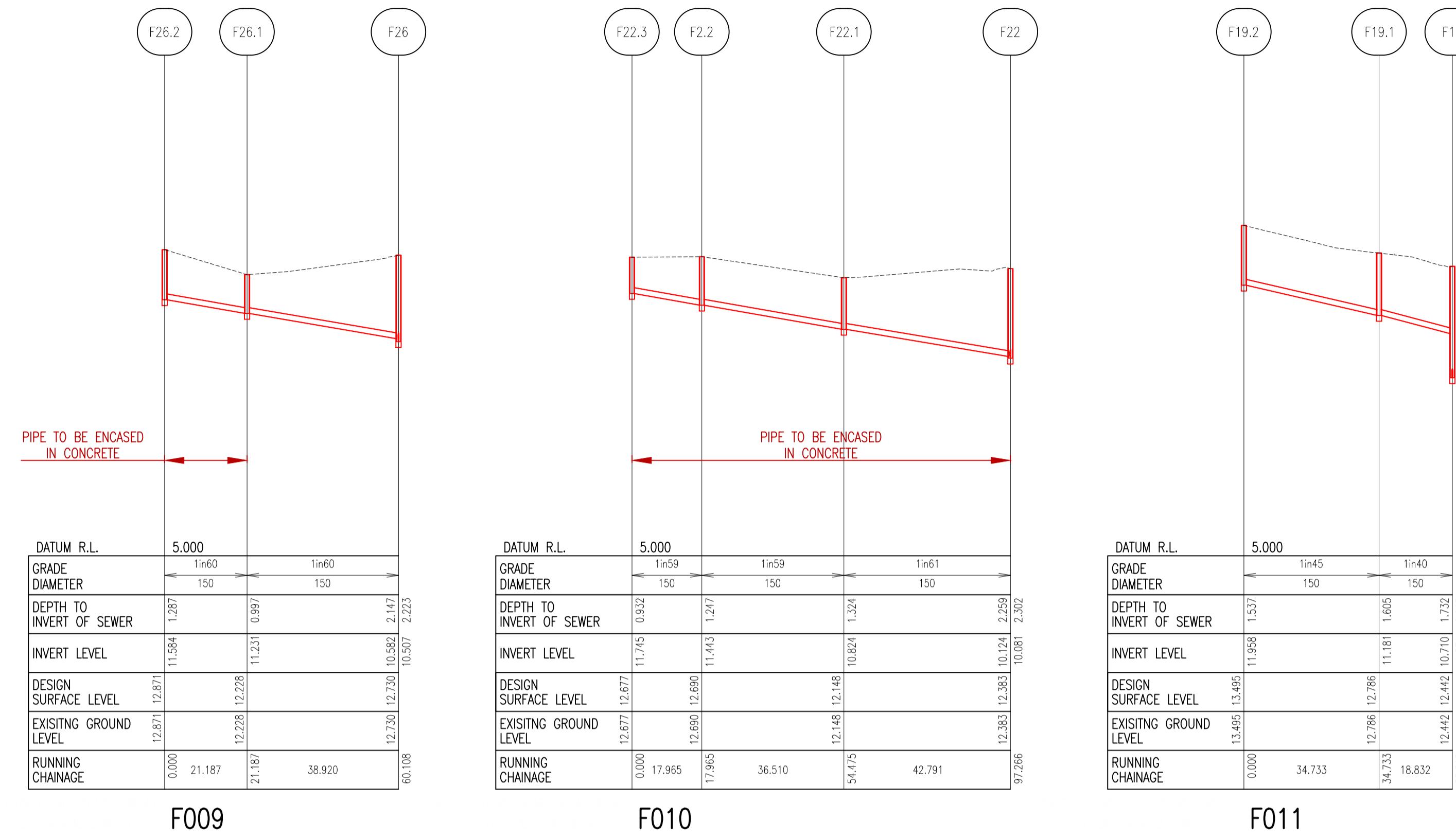
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SHEET 1 OF 3

DESIGNED APPROVED DATE

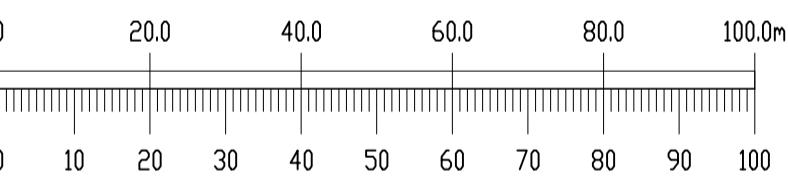
DESIGNED NS	APPROVED MD	DATE JAN 22'
JOB NO. 18-091	DRG. NO. P240	REVISION

NOTES:

- 1. DO NOT SCALE. USE FIGURED DIMENSIONS ONLY.
- 2. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL OTHER RELEVANT ARCHITECTURAL AND ENGINEERING DRAWINGS.



NOTE:
WHERE COVER TO PIPE IS LESS THAN 1.2M
PIPE SHALL BE ENCASED IN CONCRETE



AMENDMENT	DRN	APPD

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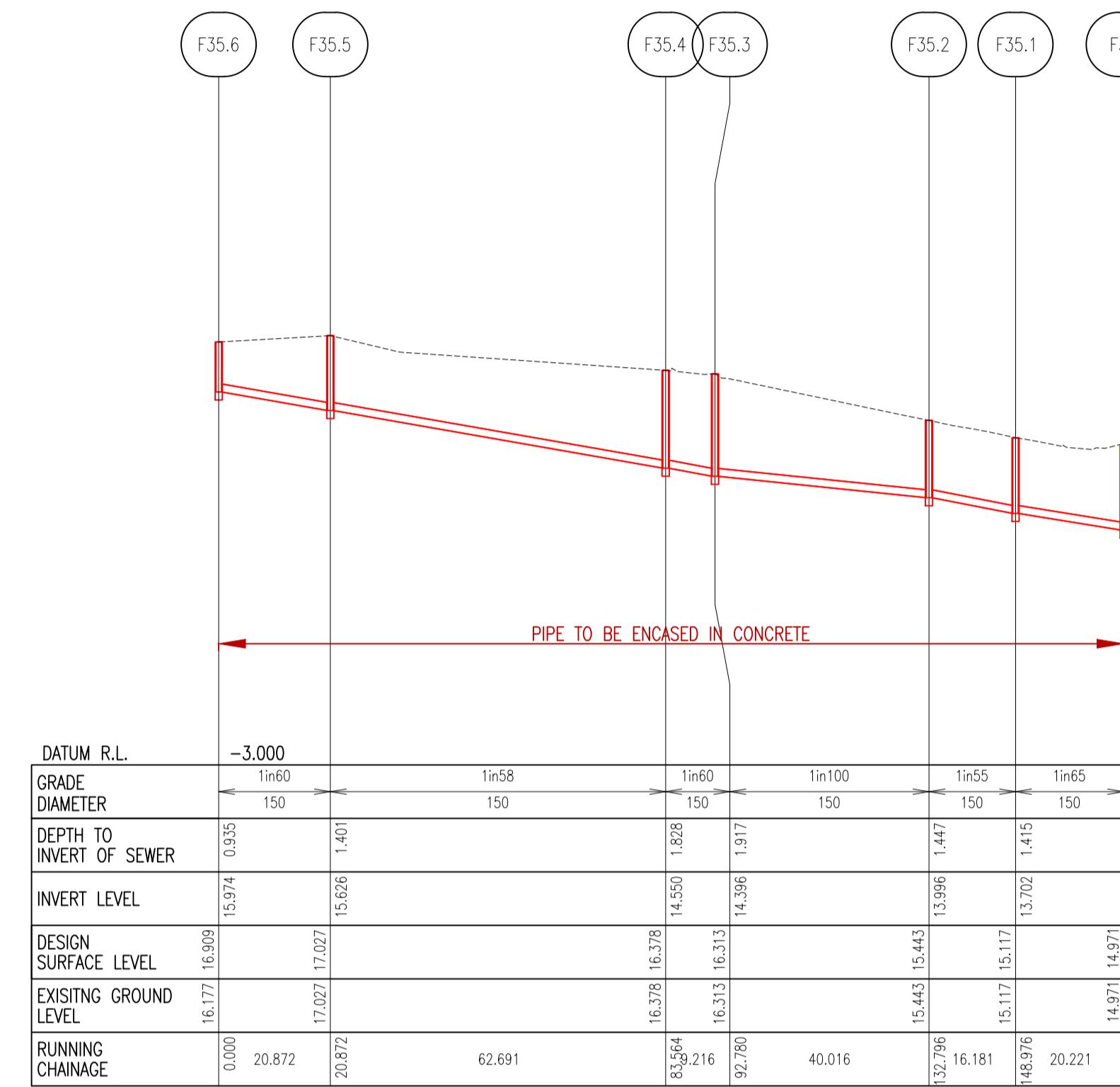
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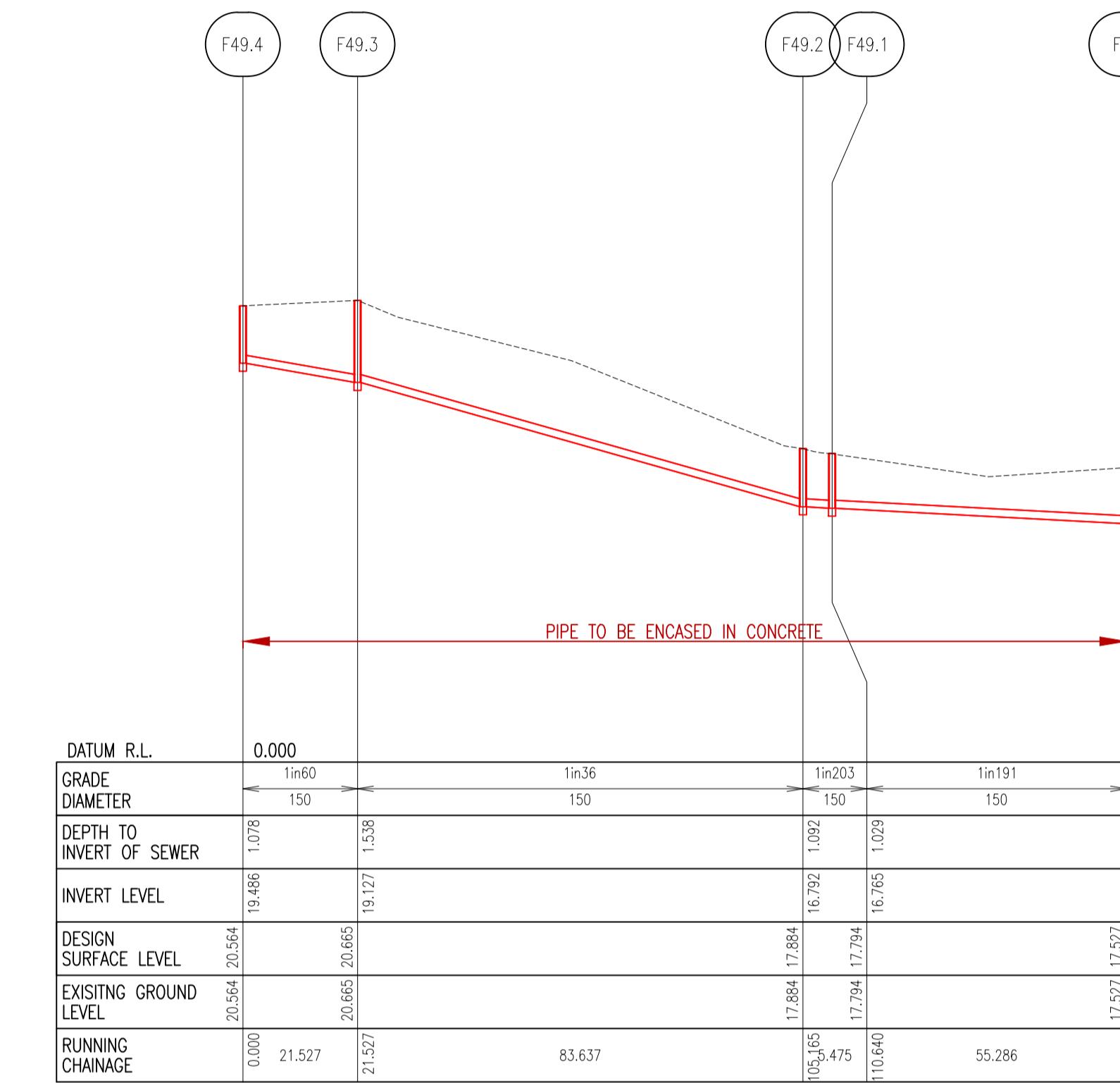
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SHEET 2 OF 3			
	DESIGNED MD	APPROVED MD	DATE JAN 22'
WN @ A1	JOB NO. 18-091	DRG. NO. P241	REVISION

NOTES:

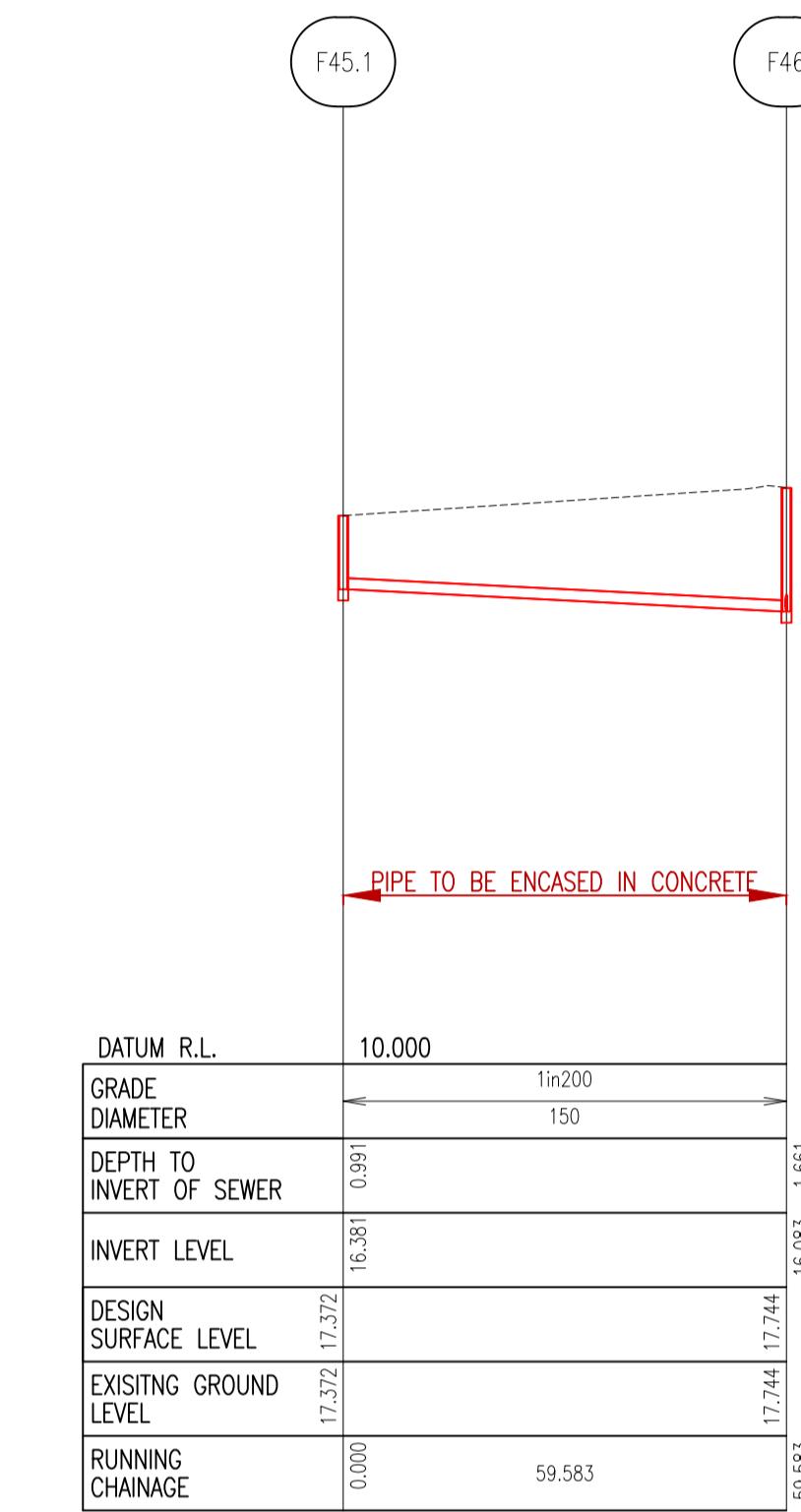
- 1. DO NOT SCALE. USE FIGURED DIMENSIONS ONLY.
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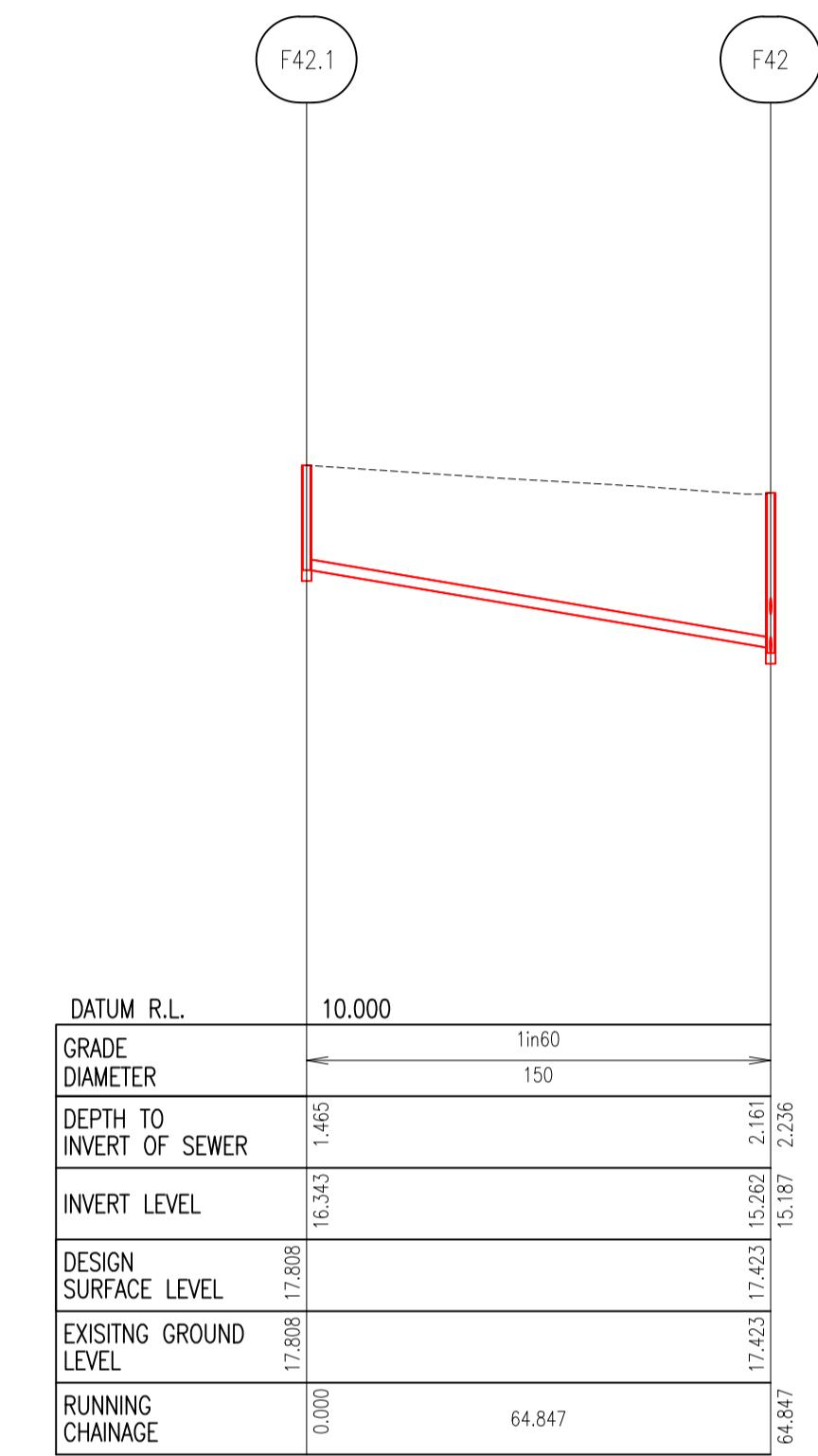
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F015



F016



F017

NOTE:
WHERE COVER TO PIPE IS LESS THAN 1.2M
PIPE SHALL BE ENCASED IN CONCRETE

REV.	DATE	AMENDMENT	DRN	APPD

**STATUS FOR PLANNING
NOT FOR CONSTRUCTION**



Waterman Moylan
Engineering Consultants

CLIENT BIRCHWELL DEVELOPMENTS LTD
ARCHITECT McCROSSAN O'ROURKE MANNING ARCHITECTS

PROJECT **BROOMFIELD SHD**

EQUI DRAINAGE LONGITUDINAL SECTIONS

PIPE DRAINAGE LONGITUDINAL SECTIONS
SHEET 3 OF 3

C. Fingal County Council SuDS Selection Checklist

Suds Measures	Measures to be used on this site	Rationale for selecting/not selecting measure	Checklist submitted? See no. 8 below
Source Control			
Swales	✓	Located on the edges of open spaces as topography allows.	
Tree Pits	✓	Roadside tree pits are to be provided throughout the development. Trees help to attenuate flows, trap silts and pollutants, promote infiltration and prevent erosion.	
Rainwater Butts			
Rainwater harvesting			
Soakaways	✓	Soakaway filters drain to partly replace static ditch on the southern boundary of the north site.	
Infiltration trenches			
Permeable pavement (Grasscrete, Block paving, Porous Asphalt etc.)	✓	All private driveways are to be permeable paving with underlying filter drains. Downpipes from the front of the houses will also drain to the filter drain under the permeable paving to facilitate maximum infiltration of surface water from driveways and roof areas.	
Green Roofs	✓	Areas of green roof are to be provided at the apartment buildings.	
Filter strips	✓	Filter drains incorporated around apartment blocks, under permeable paving and in open spaces as appropriate.	
Bio-retention systems/Raingardens			
Blue Roofs			
Filter Drain	✓	Filter drains are to be incorporated around the perimeter of each apartment block to allow for infiltration of surface water.	
Site Control			
Detention Basins			
Retention basins			
Regional Control			
Ponds			
Wetlands			
Other			
Petrol/Oil interceptor	✓	A Class 1 petrol interceptor will be provided before the surface water outfall to the public surface water network.	
Attenuation tank – only as a last resort where other measures are not feasible	✓	Attenuation tanks to be utilised throughout the development. Detention basins are not considered as a feasible option. Privately managed and maintained attenuation tanks will be utilised for the apartment blocks. Storage for all tanks is designed to have capacity for greater than the 1-in-100-year	

		storm plus 20% for climate change. All outflows will be limited to greenfield rates (or allowable) via hydrobrake system	
Oversized pipes– only as a last resort where other measures are not feasible			

Note:

1. Fingal has a preference for above ground Green Infrastructure rather than tanks or oversized pipes . Above ground flows through swales, basins etc are encouraged.
2. Demonstrate SUDS system will have sufficient Pollutant removal efficiency in accordance with Ciria Suds Manual C753
3. Basins sides should be no steeper than 1:4 and no deeper than 1.2m in the 1%AEP
4. Culverting shall be avoided where possible
5. De-culverting is encouraged.
6. Please submit evidence of infiltration rates
7. To account for climate change in the design of the drainage system rainfall intensities should be factored up by 20%
8. The Applicant must provide Suds checklists in accordance with the Appendix B of the Ciria Suds manual C753

Appendix	Name
B3	Full planning
B4	Scheme design
B5	Health and safety
B6	Infiltration assessment
B7	Proprietary treatment
B9	filter strip
B11	filter drain
B13	swale
B15	bioretention
B16	pervious pavement
B17	attenuation tank
B19	basin
B21	pond wetland

Flood risk to be assessed

Flood risk	Applicable to subject site	Measures to reduce risk	Residual risk
Fluvial			
Pluvial			
Coastal			
Groundwater			
Dam/Embankment/Canal bank breach			
Network drainage			
Snow melt			
Watermain burst			

Note:

Models should consider the risk when outlets are surcharged

Climate Change scenarios to be considered both MRFS and HEFS

D. GDSDS Attenuation Calculations



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Calculation By:

RW

Approved by:

SDN

Project Data

Catchment	North Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	13,481m ²
Paved Area	Total	47%	6,336m ²
	Drained	90%	5,702m ²
Soil Area	Total	53%	7,145m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.01348km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.009\text{m}^3/\text{s}$$

$$Q_{BARrural} = 8.995 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	7.65	18.89	23.39
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	8.99	8.99	8.99

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Calculation By:

RW

Approved by:

SDN

Summary

Catchment North Catchment 1

Project Name Broomfield, Malahide

Project Number 18-091

Client Birchwell Developments Ltd.

Architect MCORM

Status Planning - Rev. B

Date 21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	19.01m³
Treatment Volume	57.02m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	31.08m ³
1-in-30-Year Storm	81.88m ³
1-in-100-Year Storm	58.41m ³
Reduction of Long-Term Storage	-17.05m ³
Volume Required	154.33m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	17.05m³
Long Term Storage <i>(Interception provided)</i>	-1.96m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	31.08m ³
1-in-30-Year Storm	81.88m ³
1-in-100-Year Storm	58.41m ³
Total	171.38m³

The maximum attenuation volume required is 171.38m³



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Calculation By:	RW
Approved by:	SDN

Criterion 1 River Protection Volume

Catchment	North Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$13481m^2 \times 0.47 \times 0.75 =$ 4,752.05m²	<i>13,481m² site area 47% of the site is paved 75% of the paved area</i>
Volume of Interception Storage	$4752.0525m^2 \times 5mm \times 0.8 =$ 19.01m³	<i>Paved area directly drained 5mm rainfall depth 80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$13481m^2 \times 0.47 \times 0.75 =$ 4,752.05m²	<i>13,481m² site area 47% of the site is paved 75% of the paved area</i>
Volume of Treatment Storage	$4752.0525m^2 \times 15mm \times 0.8 =$ 57.02m³	<i>Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces</i>



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Calculation By: RW
Approved by: SDN

Criterion 2

River Regime Protection

Catchment	North Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	22.81	0.00	22.81	41.1	8.99	16.2	13.81	24.9
1	33.33	15.21	0.00	15.21	54.7	8.99	32.4	6.21	22.4
2	21.83	9.96	0.00	9.96	71.7	8.99	64.8	0.97	7.0
4	14.75	6.73	0.00	6.73	96.9	6.73	96.9	0.00	0.0
6	11.83	5.40	0.00	5.40	116.6	5.40	116.6	0.00	0.0
12	7.50	3.42	0.00	3.42	147.8	3.42	147.8	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	61.43	0.00	61.43	110.6	8.99	11.9	52.44	69.5
1	84.43	38.52	0.00	38.52	138.7	8.99	24.8	29.52	81.4
2	52.22	23.82	0.00	23.82	171.5	8.99	49.7	14.83	81.9
4	32.23	14.70	0.00	14.70	211.7	8.99	90.3	5.71	57.3
6	25.18	11.49	0.00	11.49	248.2	8.99	104.6	2.49	29.0
12	15.74	7.18	0.00	7.18	310.2	7.18	0.0	0.00	0.0

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	85.16	0.00	85.16	153.3	8.99	3.6	76.16	30.3
1	116.67	53.22	0.00	53.22	191.6	8.99	10.7	44.23	52.5
2	70.00	31.93	0.00	31.93	229.9	8.99	22.9	22.94	58.4
4	42.50	19.39	0.00	19.39	279.2	8.99	37.1	10.39	42.9
6	32.78	14.95	0.00	14.95	323.0	8.99	33.1	5.96	21.9
12	20.00	9.12	0.00	9.12	394.2	8.99	-7,053.8	0.13	-101.2



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Calculation By:

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Approved by:

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Criterion 4 **River Flood Protection**

Catchment	North Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol _{XS}	=	... Extra runoff volume of development over Greenfield runoff
RD	=	71 mm ... Rainfall depth of the 100 year, 6 hour event mm
A	=	1.348 Ha ... Area of site
PIMP	=	47% ... Impermeable area of total site
$\alpha 0.8$	=	90% ... Proportion of paved area drained to drainage network or river with 80% runoff
β	=	60% ... Proportion of pervious area drained to the network or river
Soil	=	0.47 ... SPR index

$$Vol_{XS} = 17.05m^3$$



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Calculation By:

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Approved by:

SDN

Project Data

Catchment	Block C
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	646m ²
Paved Area	Total	100%	646m ²
	Drained	100%	646m ²
Soil Area	Total	0%	0m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.00065km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.000m^3/s$$

$$Q_{BARrural} = 0.431 l/s$$

$$Q_{BARrural} = 30.960 l/s/Ha$$

... Note: where greenfield runoff value is <2l/s, a value of 2l/s shall be taken

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	1.70	4.20	5.20
Q _{BAR} (l/s/Ha)	26.32	65.02	80.50
Allowable Discharge	2.00	2.00	2.00

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4

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Calculation By:

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Approved by:

SDN

Summary

Catchment	Block C
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	1.94m³
Treatment Volume	5.81m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	1.31m ³
1-in-30-Year Storm	7.88m ³
1-in-100-Year Storm	5.58m ³
Reduction of Long-Term Storage	-15.09m ³
Volume Required	-0.32m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	15.09m³
Long Term Storage <i>(Interception provided)</i>	13.16m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	1.31m ³
1-in-30-Year Storm	7.88m ³
1-in-100-Year Storm	5.58m ³
Total	14.77m³

The maximum attenuation volume required is 14.77m³



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Calculation By:	RW
Approved by:	SDN

Criterion 1 River Protection Volume

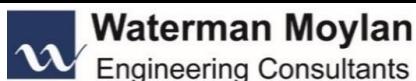
Catchment	Block C
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$646m^2 \times 1 \times 0.75 =$ 484.50m ²	<i>646m² site area 100% of the site is paved 75% of the paved area</i>
Volume of Interception Storage	$484.5m^2 \times 5mm \times 0.8 =$ 1.94m ³	<i>Paved area directly drained 5mm rainfall depth 80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$646m^2 \times 1 \times 0.75 =$ 484.50m ²	<i>646m² site area 100% of the site is paved 75% of the paved area</i>
Volume of Treatment Storage	$484.5m^2 \times 15mm \times 0.8 =$ 5.81m ³	<i>Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces</i>



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Calculation By: RW
Approved by: SDN

Criterion 2

River Regime Protection

Catchment	Block C
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period									
(Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	2.58	0.00	2.58	4.7	2.00	3.6	0.58	1.1
1	33.33	1.72	0.00	1.72	6.2	1.72	6.2	0.00	0.0
2	21.83	1.13	0.00	1.13	8.1	1.13	8.1	0.00	0.0
4	14.75	0.76	0.00	0.76	11.0	0.76	11.0	0.00	0.0
6	11.83	0.61	0.00	0.61	13.2	0.61	13.2	0.00	0.0
12	7.50	0.39	0.00	0.39	16.7	0.39	16.7	0.00	0.0

30-Year Return Period									
(Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	6.96	0.00	6.96	12.5	2.00	3.2	4.96	7.9
1	84.43	4.36	0.00	4.36	15.7	2.00	6.3	2.36	7.5
2	52.22	2.70	0.00	2.70	19.4	2.00	11.4	0.70	4.0
4	32.23	1.67	0.00	1.67	24.0	1.67	0.0	0.00	0.0
6	25.18	1.30	0.00	1.30	28.1	1.30	0.0	0.00	0.0
12	15.74	0.81	0.00	0.81	35.1	0.81	0.0	0.00	0.0

100-Year Return Period									
(Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	9.65	0.00	9.65	17.4	2.00	1.3	7.65	4.8
1	116.67	6.03	0.00	6.03	21.7	2.00	2.8	4.03	5.6
2	70.00	3.62	0.00	3.62	26.0	2.00	3.4	1.62	2.7
4	42.50	2.20	0.00	2.20	31.6	2.00	-62.1	0.20	-6.1
6	32.78	1.69	0.00	1.69	36.6	1.69	0.0	0.00	0.0
12	20.00	1.03	0.00	1.03	44.7	1.03	0.0	0.00	0.0



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Calculation By:

RW

Approved by:

SDN

Criterion 4 **River Flood Protection**

Catchment	Block C
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS}

... Extra runoff volume of development over Greenfield runoff

RD = 71 mm

... Rainfall depth of the 100 year, 6 hour event mm

A = 0.065 Ha

... Area of site

PIMP = 100%

... Impermeable area of total site

$\alpha 0.8$ = 100%

... Proportion of paved area drained to drainage network or river with 80% runoff

β = 60%

... Proportion of pervious area drained to the network or river

Soil = 0.47

... SPR index

$$Vol_{XS} = 15.09m^3$$



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Calculation By:

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Approved by:

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Project Data

Catchment	North Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	15,684m ²
Paved Area	Total	81%	12,704m ²
	Drained	90%	11,434m ²
Soil Area	Total	19%	2,980m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.01568km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.010\text{m}^3/\text{s}$$

$$Q_{BARrural} = 10.465 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

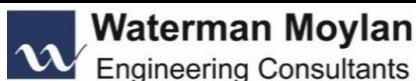
Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	8.90	21.98	27.21
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	10.46	10.46	10.46

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Calculation By:

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Summary

Catchment	North Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	38.11m³
Treatment Volume	114.34m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	90.11m ³
1-in-30-Year Storm	201.67m ³
1-in-100-Year Storm	147.80m ³
Reduction of Long-Term Storage	-185.20m ³
Volume Required	254.39m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage (no interception provided)	185.20m³
Long Term Storage (Interception provided)	147.08m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	90.11m ³
1-in-30-Year Storm	201.67m ³
1-in-100-Year Storm	147.80m ³
Total	439.58m³

The maximum attenuation volume required is 439.58m³



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Calculation By:	RW
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Criterion 1 River Protection Volume

Catchment	North Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$15684m^2 \times 0.81 \times 0.75 =$ 9,528.03m ²	<i>15,684m² site area 81% of the site is paved 75% of the paved area</i>
Volume of Interception Storage	$9528.03m^2 \times 5mm \times 0.8 =$ 38.11m³	<i>Paved area directly drained 5mm rainfall depth 80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$15684m^2 \times 0.81 \times 0.75 =$ 9,528.03m ²	<i>15,684m² site area 81% of the site is paved 75% of the paved area</i>
Volume of Treatment Storage	$9528.03m^2 \times 15mm \times 0.8 =$ 114.34m³	<i>Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces</i>



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Calculation By: RW
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Criterion 2

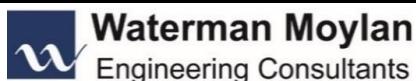
River Regime Protection

Catchment	North Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	45.73	0.00	45.73	82.3	10.46	18.8	35.27	63.5
1	33.33	30.49	0.00	30.49	109.8	10.46	37.7	20.02	72.1
2	21.83	19.97	0.00	19.97	143.8	10.46	75.3	9.51	68.4
4	14.75	13.49	0.00	13.49	194.3	10.46	150.7	3.03	43.6
6	11.83	10.82	0.00	10.82	233.8	10.46	226.0	0.36	7.8
12	7.50	6.86	0.00	6.86	296.4	6.86	296.4	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	123.18	0.00	123.18	221.7	10.46	12.1	112.71	130.8
1	84.43	77.23	0.00	77.23	278.0	10.46	26.4	66.77	168.3
2	52.22	47.76	0.00	47.76	343.9	10.46	55.1	37.30	196.5
4	32.23	29.48	0.00	29.48	424.5	10.46	111.0	19.01	201.7
6	25.18	23.03	0.00	23.03	497.6	10.46	166.0	12.57	199.4
12	15.74	14.40	0.00	14.40	622.0	10.46	260.3	3.93	97.9

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	170.74	0.00	170.74	307.3	10.46	1.0	160.28	14.7
1	116.67	106.71	0.00	106.71	384.2	10.46	7.9	96.25	72.7
2	70.00	64.03	0.00	64.03	461.0	10.46	21.9	53.56	111.9
4	42.50	38.87	0.00	38.87	559.8	10.46	49.9	28.41	135.3
6	32.78	29.98	0.00	29.98	647.6	10.46	79.3	19.52	147.8
12	20.00	18.29	0.00	18.29	790.3	10.46	86.2	7.83	64.5



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Criterion 4 River Flood Protection

Catchment	North Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol _{XS}	=	RD x A x 10 [(PIMP/100 x α0.8) + (1 - (PIMP/100))(β x Soil) - Soil]
Vol _{XS}	=	... Extra runoff volume of development over Greenfield runoff
RD	=	71 mm ... Rainfall depth of the 100 year, 6 hour event mm
A	=	1.568 Ha ... Area of site
PIMP	=	81% ... Impermeable area of total site
α0.8	=	90% ... Proportion of paved area drained to drainage network or river with 80% runoff
β	=	60% ... Proportion of pervious area drained to the network or river
Soil	=	0.47 ... SPR index

$$Vol_{XS} = 185.20m^3$$



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Project Data

Catchment	Blocks A & B
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	4,126m ²
Paved Area	Total	100%	4,126m ²
	Drained	100%	4,126m ²
Soil Area	Total	0%	0m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.00413km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.003\text{m}^3/\text{s}$$

$$Q_{BARrural} = 2.753 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	2.34	5.78	7.16
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	2.75	2.75	2.75

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Calculation By:

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Approved by:

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Summary

Catchment	Blocks A & B
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	12.38m³
Treatment Volume	37.13m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	40.08m ³
1-in-30-Year Storm	88.02m ³
1-in-100-Year Storm	54.15m ³
Reduction of Long-Term Storage	-96.40m ³
Volume Required	85.85m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	96.40m³
Long Term Storage <i>(Interception provided)</i>	84.02m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	40.08m ³
1-in-30-Year Storm	88.02m ³
1-in-100-Year Storm	54.15m ³
Total	182.25m³

The maximum attenuation volume required is 182.25m³



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Criterion 1 River Protection Volume

Catchment	Blocks A & B
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$4126m^2 \times 1 \times 0.75 =$ 3,094.50m ²	<i>4,126m² site area 100% of the site is paved 75% of the paved area</i>
Volume of Interception Storage	$3094.5m^2 \times 5mm \times 0.8 =$ 12.38m³	<i>Paved area directly drained 5mm rainfall depth 80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$4126m^2 \times 1 \times 0.75 =$ 3,094.50m ²	<i>4,126m² site area 100% of the site is paved 75% of the paved area</i>
Volume of Treatment Storage	$3094.5m^2 \times 15mm \times 0.8 =$ 37.13m³	<i>Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces</i>



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Calculation By: RW
Approved by: SDN

Criterion 2

River Regime Protection

Catchment	Blocks A & B
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	16.50	0.00	16.50	29.7	2.75	5.0	13.75	24.8
1	33.33	11.00	0.00	11.00	39.6	2.75	9.9	8.25	29.7
2	21.83	7.21	0.00	7.21	51.9	2.75	19.8	4.45	32.1
4	14.75	4.87	0.00	4.87	70.1	2.75	39.6	2.12	30.5
6	11.83	3.91	0.00	3.91	84.4	2.75	59.5	1.15	24.9
12	7.50	2.48	0.00	2.48	106.9	2.48	106.9	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	44.45	0.00	44.45	80.0	2.75	2.8	41.70	43.0
1	84.43	27.87	0.00	27.87	100.3	2.75	6.4	25.12	58.4
2	52.22	17.24	0.00	17.24	124.1	2.75	13.7	14.48	72.2
4	32.23	10.64	0.00	10.64	153.2	2.75	28.4	7.88	81.5
6	25.18	8.31	0.00	8.31	179.6	2.75	43.6	5.56	88.0
12	15.74	5.20	0.00	5.20	224.5	2.75	82.8	2.44	73.5

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	61.61	0.00	61.61	110.9	2.75	-0.7	58.86	-14.1
1	116.67	38.51	0.00	38.51	138.6	2.75	0.7	35.76	8.6
2	70.00	23.11	0.00	23.11	166.4	2.75	3.6	20.35	26.5
4	42.50	14.03	0.00	14.03	202.0	2.75	10.3	11.28	42.3
6	32.78	10.82	0.00	10.82	233.7	2.75	18.5	8.07	54.1
12	20.00	6.60	0.00	6.60	285.2	2.75	33.0	3.85	46.2



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Calculation By:

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Criterion 4 River Flood Protection

Catchment	Blocks A & B
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS}

... Extra runoff volume of development over Greenfield runoff

$RD = 71 \text{ mm}$

... Rainfall depth of the 100 year, 6 hour event mm

$A = 0.413 \text{ Ha}$

... Area of site

$PIMP = 100\%$

... Impermeable area of total site

$\alpha 0.8 = 100\%$

... Proportion of paved area drained to drainage network or river with 80% runoff

$\beta = 60\%$

... Proportion of pervious area drained to the network or river

$Soil = 0.47$

... SPR index

$$Vol_{XS} = 96.40 \text{ m}^3$$



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Project Data

Catchment	North Catchment 3
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	27,907m ²
Paved Area	Total	59%	16,465m ²
	Drained	90%	14,819m ²
Soil Area	Total	41%	11,442m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.02791km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.019\text{m}^3/\text{s}$$

$$Q_{BARrural} = 18.620 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	15.83	39.10	48.41
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	18.62	18.62	18.62

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Calculation By:

RW

Approved by:

SDN

Summary

Catchment North Catchment 3

Project Name Broomfield, Malahide

Project Number 18-091

Client Birchwell Developments Ltd.

Architect MCORM

Status Planning - Rev. B

Date 21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	49.40m³
Treatment Volume	148.19m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	94.03m ³
1-in-30-Year Storm	236.40m ³
1-in-100-Year Storm	151.79m ³
Reduction of Long-Term Storage	-139.14m ³
Volume Required	343.09m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	139.14m³
Long Term Storage <i>(Interception provided)</i>	89.74m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	94.03m ³
1-in-30-Year Storm	236.40m ³
1-in-100-Year Storm	151.79m ³
Total	482.23m³

The maximum attenuation volume required is 482.23m³



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Approved by:	SDN

Criterion 1 River Protection Volume

Catchment	North Catchment 3
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$27907m^2 \times 0.59 \times 0.75 =$ 12,348.85m ²	27,907m ² site area 59% of the site is paved 75% of the paved area
Volume of Interception Storage	$12348.8475m^2 \times 5mm \times 0.8 =$ 49.40m ³	Paved area directly drained 5mm rainfall depth 80% paved runoff factor

1.2 Treatment Volume

Paved surfaces draining to river	$27907m^2 \times 0.59 \times 0.75 =$ 12,348.85m ²	27,907m ² site area 59% of the site is paved 75% of the paved area
Volume of Treatment Storage	$12348.8475m^2 \times 15mm \times 0.8 =$ 148.19m ³	Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces



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Criterion 2

River Regime Protection

Catchment	North Catchment 3
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	59.27	0.00	59.27	106.7	18.62	33.5	40.65	73.2
1	33.33	39.52	0.00	39.52	142.3	18.62	67.0	20.90	75.2
2	21.83	25.88	0.00	25.88	186.4	18.62	134.1	7.26	52.3
4	14.75	17.49	0.00	17.49	251.8	17.49	251.8	0.00	0.0
6	11.83	14.03	0.00	14.03	303.0	14.03	303.0	0.00	0.0
12	7.50	8.89	0.00	8.89	384.1	8.89	384.1	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	159.65	0.00	159.65	287.4	18.62	23.6	141.03	178.6
1	84.43	100.09	0.00	100.09	360.3	18.62	49.8	81.47	218.1
2	52.22	61.90	0.00	61.90	445.7	18.62	101.7	43.28	236.4
4	32.23	38.20	0.00	38.20	550.1	18.62	196.6	19.58	206.8
6	25.18	29.85	0.00	29.85	644.9	18.62	277.5	11.23	167.4
12	15.74	18.66	0.00	18.66	806.2	18.62	-33,195.5	0.04	-73.4

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	221.29	0.00	221.29	398.3	18.62	4.9	202.67	53.2
1	116.67	138.31	0.00	138.31	497.9	18.62	18.6	119.69	119.2
2	70.00	82.98	0.00	82.98	597.5	18.62	43.9	64.36	151.8
4	42.50	50.38	0.00	50.38	725.5	18.62	85.4	31.76	145.8
6	32.78	38.86	0.00	38.86	839.3	18.62	115.5	20.24	125.5
12	20.00	23.71	0.00	23.71	1,024.3	18.62	-335.7	5.09	-91.8



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Criterion 4 River Flood Protection

Catchment	North Catchment 3
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol _{XS}	=	RD x A x 10 [(PIMP/100 x α0.8) + (1 - (PIMP/100))(β x Soil) - Soil]
Vol _{XS}	=	... Extra runoff volume of development over Greenfield runoff
RD	=	71 mm ... Rainfall depth of the 100 year, 6 hour event mm
A	=	2.791 Ha ... Area of site
PIMP	=	59% ... Impermeable area of total site
α0.8	=	90% ... Proportion of paved area drained to drainage network or river with 80% runoff
β	=	60% ... Proportion of pervious area drained to the network or river
Soil	=	0.47 ... SPR index

$$Vol_{XS} = 139.14m^3$$



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Project Data

Catchment	North Catchment 4
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Development Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	19,827m ²
Paved Area	Total	56%	11,103m ²
	Drained	90%	9,993m ²
Soil Area	Total	44%	8,724m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.01983km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.013\text{m}^3/\text{s}$$

$$Q_{BARrural} = 13.229 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

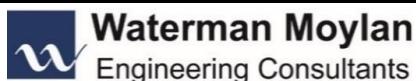
Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	11.24	27.78	34.40
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	13.23	13.23	13.23

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Calculation By:

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Summary

Catchment North Catchment 4

Project Name Broomfield, Malahide

Project Number 18-091

Client Birchwell Development Ltd.

Architect MCORM

Status Planning - Rev. B

Date 21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	33.31m³
Treatment Volume	99.93m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	60.38m ³
1-in-30-Year Storm	157.00m ³
1-in-100-Year Storm	102.36m ³
Reduction of Long-Term Storage	-80.41m ³
Volume Required	239.33m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	80.41m³
Long Term Storage <i>(Interception provided)</i>	47.10m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	60.38m ³
1-in-30-Year Storm	157.00m ³
1-in-100-Year Storm	102.36m ³
Total	319.74m³

The maximum attenuation volume required is 319.74m³



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Calculation By: RW
Approved by: SDN

Criterion 1 River Protection Volume

Catchment	North Catchment 4
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Development Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$19827m^2 \times 0.56 \times 0.75 =$ 8,327.34m ²	19,827m ² site area 56% of the site is paved 75% of the paved area
Volume of Interception Storage	$8327.34m^2 \times 5mm \times 0.8 =$ 33.31m ³	Paved area directly drained 5mm rainfall depth 80% paved runoff factor

1.2 Treatment Volume

Paved surfaces draining to river	$19827m^2 \times 0.56 \times 0.75 =$ 8,327.34m ²	19,827m ² site area 56% of the site is paved 75% of the paved area
Volume of Treatment Storage	$8327.34m^2 \times 15mm \times 0.8 =$ 99.93m ³	Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces



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Criterion 2

River Regime Protection

Catchment	North Catchment 4
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Development Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	39.97	0.00	39.97	71.9	13.23	23.8	26.74	48.1
1	33.33	26.65	0.00	26.65	95.9	13.23	47.6	13.42	48.3
2	21.83	17.45	0.00	17.45	125.7	13.23	95.2	4.22	30.4
4	14.75	11.79	0.00	11.79	169.8	11.79	169.8	0.00	0.0
6	11.83	9.46	0.00	9.46	204.3	9.46	204.3	0.00	0.0
12	7.50	6.00	0.00	6.00	259.0	6.00	259.0	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	107.66	0.00	107.66	193.8	13.23	17.0	94.43	121.7
1	84.43	67.50	0.00	67.50	243.0	13.23	35.8	54.27	147.1
2	52.22	41.74	0.00	41.74	300.6	13.23	72.8	28.51	157.0
4	32.23	25.76	0.00	25.76	371.0	13.23	139.5	12.53	132.2
6	25.18	20.13	0.00	20.13	434.9	13.23	193.2	6.90	100.8
12	15.74	12.58	0.00	12.58	543.6	12.58	0.0	0.00	0.0

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	149.23	0.00	149.23	268.6	13.23	3.8	136.00	39.5
1	116.67	93.27	0.00	93.27	335.8	13.23	13.7	80.04	82.8
2	70.00	55.96	0.00	55.96	402.9	13.23	31.7	42.73	102.4
4	42.50	33.98	0.00	33.98	489.2	13.23	59.6	20.75	93.4
6	32.78	26.20	0.00	26.20	566.0	13.23	76.4	12.97	74.9
12	20.00	15.99	0.00	15.99	690.7	13.23	-412.8	2.76	-86.1



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Criterion 4 **River Flood Protection**

Catchment	North Catchment 4
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Development Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS}

... Extra runoff volume of development over Greenfield runoff

RD = 71 mm

... Rainfall depth of the 100 year, 6 hour event mm

A = 1.983 Ha

... Area of site

PIMP = 56%

... Impermeable area of total site

$\alpha 0.8$ = 90%

... Proportion of paved area drained to drainage network or river with 80% runoff

β = 60%

... Proportion of pervious area drained to the network or river

Soil = 0.47

... SPR index

$$Vol_{XS} = 80.41m^3$$



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Calculation By:

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Project Data

Catchment	South Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	08/06/2021

Description		%	Area
Total Site Area		-	9,584m ²
Paved Area	Total	53%	5,080m ²
	Drained	90%	4,572m ²
Soil Area	Total	47%	4,504m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.00958km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.006\text{m}^3/\text{s}$$

$$Q_{BARrural} = 6.395 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	5.44	13.43	16.63
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	6.39	6.39	6.39

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Summary

Catchment	South Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	08/06/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	15.24m³
Treatment Volume	45.72m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	26.76m ³
1-in-30-Year Storm	70.05m ³
1-in-100-Year Storm	46.83m ³
Reduction of Long-Term Storage	-29.95m ³
Volume Required	113.68m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage (no interception provided)	29.95m³
Long Term Storage (Interception provided)	14.71m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	26.76m ³
1-in-30-Year Storm	70.05m ³
1-in-100-Year Storm	46.83m ³
Total	143.63m³

The maximum attenuation volume required is 143.63m³



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Criterion 1 River Protection Volume

Catchment	South Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	08/06/2021

1.1 Interception

Paved surfaces connected to drainage system	$9584m^2 \times 0.53 \times 0.75 =$ 3,809.64m ²	9,584m ² site area 53% of the site is paved 75% of the paved area
Volume of Interception Storage	$3809.64m^2 \times 5mm \times 0.8 =$ 15.24m ³	Paved area directly drained 5mm rainfall depth 80% paved runoff factor

1.2 Treatment Volume

Paved surfaces draining to river	$9584m^2 \times 0.53 \times 0.75 =$ 3,809.64m ²	9,584m ² site area 53% of the site is paved 75% of the paved area
Volume of Treatment Storage	$3809.64m^2 \times 15mm \times 0.8 =$ 45.72m ³	Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces



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Criterion 2

River Regime Protection

Catchment	South Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	08/06/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	18.29	0.00	18.29	32.9	6.39	11.5	11.89	21.4
1	33.33	12.19	0.00	12.19	43.9	6.39	23.0	5.80	20.9
2	21.83	7.99	0.00	7.99	57.5	6.39	46.0	1.59	11.4
4	14.75	5.39	0.00	5.39	77.7	6.39	77.7	0.00	0.0
6	11.83	4.33	0.00	4.33	93.5	4.33	93.5	0.00	0.0
12	7.50	2.74	0.00	2.74	118.5	2.74	118.5	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	49.25	0.00	49.25	88.7	6.39	8.3	42.86	55.7
1	84.43	30.88	0.00	30.88	111.2	6.39	17.4	24.48	66.7
2	52.22	19.10	0.00	19.10	137.5	6.39	35.3	12.70	70.1
4	32.23	11.79	0.00	11.79	169.7	6.39	66.7	5.39	56.2
6	25.18	9.21	0.00	9.21	198.9	6.39	89.5	2.82	39.4
12	15.74	5.76	0.00	5.76	248.7	5.76	0.0	0.00	0.0

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	68.27	0.00	68.27	122.9	6.39	2.1	61.87	19.9
1	116.67	42.67	0.00	42.67	153.6	6.39	6.9	36.27	39.1
2	70.00	25.60	0.00	25.60	184.3	6.39	15.6	19.21	46.8
4	42.50	15.54	0.00	15.54	223.8	6.39	28.2	9.15	40.3
6	32.78	11.99	0.00	11.99	258.9	6.39	33.6	5.59	29.4
12	20.00	7.31	0.00	7.31	316.0	6.39	-359.6	0.92	-51.7



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Calculation By:

RW

Approved by:

SDN

Criterion 4 **River Flood Protection**

Catchment	South Catchment 1
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	08/06/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS}

... Extra runoff volume of development over Greenfield runoff

RD = 71 mm

... Rainfall depth of the 100 year, 6 hour event mm

A = 0.958 Ha

... Area of site

PIMP = 53%

... Impermeable area of total site

$\alpha 0.8$ = 90%

... Proportion of paved area drained to drainage network or river with 80% runoff

β = 60%

... Proportion of pervious area drained to the network or river

Soil = 0.47

... SPR index

$$Vol_{XS} = 29.95m^3$$



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Project Data

Catchment	South Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

Description		%	Area
Total Site Area		-	19,193m ²
Paved Area	Total	52%	9,980m ²
	Drained	90%	8,982m ²
Soil Area	Total	48%	9,213m ²
	Drained	0%	0m ²

Soil Type:	Type 4
SPR Index (from FSR):	0.47
SAAR:	923mm
Rain Data:	Dublin Airport
Climate Change Factor:	20%

Greenfield Runoff:

$$Q_{BARrural} = 0.00108 \times \text{Area}^{0.89} \times \text{SAAR}^{1.17} \times \text{Soil}^{2.17}$$

Area = 0.01919km² ... Total site area in km²

SAAR = 923mm ... Standard Average Annual Rainfall in mm

SOIL = 0.47 ... The "SPR" index from FSR

Note: Where a site is <0.5km², the Q_{BARrural} formula should be applied for 0.5km² and the result factored based on the ratio of the actual site area and the applied area.

$$Q_{BARrural} = 0.013\text{m}^3/\text{s}$$

$$Q_{BARrural} = 12.806 \text{ l/s}$$

$$Q_{BARrural} = 6.672 \text{ l/s/Ha}$$

Return Period	1-year	30-year	100-year
Growth Factor	0.85	2.10	2.60
Q _{BAR} (l/s)	10.89	26.89	33.30
Q _{BAR} (l/s/Ha)	5.67	14.01	17.35
Allowable Discharge	12.81	12.81	12.81

Rainfall Data:

Rain Data From: Dublin Airport

Climate Change Factor: 20%

Duration (Hours)	Return Period (Years)						
	1	5	10	20	30	50	100
0.5	9.0	14.4	17.9	22.0	24.2	28.8	33.6
1	12.0	18.6	22.9	27.6	30.4	36.0	42.0
2	15.7	23.8	28.8	34.8	37.6	43.2	50.4
4	21.2	31.2	37.2	43.2	46.4	52.8	61.2
6	25.6	37.2	43.2	50.4	54.4	62.4	70.8
12	32.4	46.8	18.0	63.6	68.0	76.8	86.4



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Summary

Catchment South Catchment 2

Project Name Broomfield, Malahide

Project Number 18-091

Client Birchwell Developments Ltd.

Architect MCORM

Status Planning - Rev. B

Date 21/09/2021

Summary of GDSDS Calculations:

Criterion 1: River Protection Volume

Interception Volume	29.94m³
Treatment Volume	89.82m³

Criterion 2: River Regime Protection

1-in-1-Year Storm	52.03m ³
1-in-30-Year Storm	136.33m ³
1-in-100-Year Storm	92.01m ³
Reduction of Long-Term Storage	-54.03m ³
Volume Required	226.34m³

... Includes head-loss correction

Criterion 4: River Flood Protection

Long Term Storage <i>(no interception provided)</i>	54.03m³
Long Term Storage <i>(Interception provided)</i>	24.09m³

Total Attenuation Volume Requirement:

1-in-100 Year Storm

1-in-1-Year Storm	52.03m ³
1-in-30-Year Storm	136.33m ³
1-in-100-Year Storm	92.01m ³
Total	280.37m³

The maximum attenuation volume required is 280.37m³



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Criterion 1 River Protection Volume

Catchment	South Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1.1 Interception

Paved surfaces connected to drainage system	$19193m^2 \times 0.52 \times 0.75 =$ 7,485.27m²	<i>19,193m² site area 52% of the site is paved 75% of the paved area</i>
Volume of Interception Storage	$7485.27m^2 \times 5mm \times 0.8 =$ 29.94m³	<i>Paved area directly drained 5mm rainfall depth 80% paved runoff factor</i>

1.2 Treatment Volume

Paved surfaces draining to river	$19193m^2 \times 0.52 \times 0.75 =$ 7,485.27m²	<i>19,193m² site area 52% of the site is paved 75% of the paved area</i>
Volume of Treatment Storage	$7485.27m^2 \times 15mm \times 0.8 =$ 89.82m³	<i>Paved area directly drained 15mm rainfall depth 80% runoff from paved surfaces</i>



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Criterion 2

River Regime Protection

Catchment	South Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

1-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	50.00	35.93	0.00	35.93	64.7	12.81	23.1	23.12	41.6
1	33.33	23.95	0.00	23.95	86.2	12.81	46.1	11.15	40.1
2	21.83	15.69	0.00	15.69	113.0	12.81	92.2	2.88	20.8
4	14.75	10.60	0.00	10.60	152.6	10.60	152.6	0.00	0.0
6	11.83	8.50	0.00	8.50	183.7	8.50	183.7	0.00	0.0
12	7.50	5.39	0.00	5.39	232.8	5.39	232.8	0.00	0.0

30-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	134.67	96.77	0.00	96.77	174.2	12.81	16.7	83.96	109.5
1	84.43	60.67	0.00	60.67	218.4	12.81	35.0	47.87	130.7
2	52.22	37.52	0.00	37.52	270.2	12.81	70.6	24.72	136.3
4	32.23	23.16	0.00	23.16	333.5	12.81	132.9	10.35	107.4
6	25.18	18.10	0.00	18.10	390.9	12.81	175.9	5.29	72.6
12	15.74	11.31	0.00	11.31	488.7	11.31	0.0	0.00	0.0

100-Year Return Period (Climate Change Factor = 20%)									
Duration	Rainfall Rate	Runoff = Rainfall Rate x Area x Soil Type				Discharge		Storage	
		Paved	Green	Total	Volume	Rate	Volume	Rate	Volume
Hours	(l/s/Ha)	l/s	l/s	l/s	m³	l/s	m³	l/s	m³
0.5	186.67	134.14	0.00	134.14	241.4	12.81	4.3	121.33	40.4
1	116.67	83.84	0.00	83.84	301.8	12.81	14.0	71.03	77.7
2	70.00	50.30	0.00	50.30	362.2	12.81	31.4	37.49	92.0
4	42.50	30.54	0.00	30.54	439.8	12.81	55.9	17.73	77.4
6	32.78	23.55	0.00	23.55	508.8	12.81	64.6	10.75	54.2
12	20.00	14.37	0.00	14.37	620.9	12.81	-902.4	1.57	-110.3



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Criterion 4 **River Flood Protection**

Catchment	South Catchment 2
Project Name	Broomfield, Malahide
Project Number	18-091
Client	Birchwell Developments Ltd.
Architect	MCORM
Status	Planning - Rev. B
Date	21/09/2021

$$Vol_{XS} = RD \times A \times 10 [(PIMP/100 \times \alpha 0.8) + (1 - (PIMP/100))(\beta \times Soil) - Soil]$$

Vol_{XS}

... Extra runoff volume of development over Greenfield runoff

RD = 71 mm

... Rainfall depth of the 100 year, 6 hour event mm

A = 1.919 Ha

... Area of site

PIMP = 52%

... Impermeable area of total site

$\alpha 0.8$ = 90%

... Proportion of paved area drained to drainage network or river with 80% runoff

β = 60%

... Proportion of pervious area drained to the network or river

Soil = 0.47

... SPR index

$$Vol_{XS} = 54.03m^3$$

UK and Ireland Office Locations

